# Chapter 8. Calculation of PFD using PDS method

### Mary Ann Lundteigen Marvin Rausand

#### RAMS Group Department of Mechanical and Industrial Engineering NTNU

(Version 0.1)



Lundteigen& Rausand

Chapter 8.Calculation of PFD using PDS method

## Learning Objectives

The main learning objectives associated with these slides are to:

- Become familiar with the attributes of PDS method
- Become familiar with how to utilize PDS data for the analysis

The slides include topics from Chapter 8 in **Reliability of Safety-Critical Systems: Theory and Applications**. DOI:10.1002/9781118776353.

### **Outline of Presentation**







### PDS in brief

Some keywords:

- > PDS is a Norwegian acronym for computerized safety-systems.
- PDS relates to a forum www.sintef.no/pds as well as the PDS method.
- Focuses primarily on the oil and gas industry.



### PDS method

The PDS method is a framework developed for calculating unavailability of safety-instrumented systems. The method is complemented by a PDS data handbook, developed jointly by PDS participants.

Some keywords:

- Focus primarily on safety-instrumented systems operating in the low-demand mode, even if some extensions have been made to also address high-demand.
- Provides formulas for calculating the critical safety unavailability (CSU), which includes PFDavg, as well as for the spurious trip rate.
- Includes an extension for how to include common cause failures (CCFs) in voted configurations

Image Critical safety unavailability (CSU) of a safety instrumented function (SIF) is the probability that hte SIF cannot be performed if a demand occurs. CSU is defined as:

 $CSU = PFD_{avg} + DTU + P_{TIF}$ 

where DTU is the downtime unavailability (due to testing and repair) and  $P_{\rm TIF}$  is the probability of a test-independent failure.

We notice already now that the PDS method (i) separates PFD from DTU (as opposed to formulas in IEC 61508) and that a new parameter  $P_{\rm TIF}$  has been added.

## DTU

Solution Solution Content in the second seco

DTU may be split into two parts:

Measure	Description
DTU <sub>R</sub>	Part of the downtime unavailability due to repair of dangerous (D) faults, resulting in a period when it is known that the SIF is unavailable.
DTU <sub>T</sub>	Part of the downtime unavailability resulting from planned activities, such as proof-testing and planned maintenance, when it is known that the SIF is unavailable.

# PFD<sub>avg</sub>

The PFD<sub>*avg*</sub> constitutes two parts:

- ► PFD<sup>(i)</sup><sub>avg</sub>: This is the "traditional formula" for PFD<sub>avg</sub> when only DU failures are included. Often, the factor  $(1 \beta)$  as this factor usually is close to 1.
- PFD<sup>(c)</sup><sub>avg</sub>: This is the "traditional formula" for including CCFs using the standard beta factor model with one exception: A C<sub>koon</sub> factor is introduced so that::

$$PFD_{avg}^{(c)} = C_{koon}\beta \frac{\lambda_{DU}\tau}{2}$$

For more in-depth presentation of the theory behind the  $C_{koon}$  factor, see the PDS method.

# Ckoon table

Values of Ckoon used in the PDS method:

k/n	n=2	n=3	n=4	n=5	n=6
k=1	1.00	0.50	0.30	0.20	0.15
k=2	-	2.00	1.10	0.80	0.60
k=3	-	-	2.80	1.60	1.20
k=4	-	-	-	3.60	1.90
k=5	-	-	-	-	4.50

It may be remarked that IEC 61508 in its most recent version (2010) has included a similar table, but with slightly different calibration of the parameters.

# Example

Consider a 1003 system. In this case the  $PFD_{avg}$  is:

$$PFD_{avg} = \frac{(\lambda_{DU}\tau)^3}{4} + C_{1oo3}\beta \frac{\lambda_{DU}\tau}{2}$$

It may be remarked that the PDS data handbooks include data for failure rates and beta values for typical SIS components.

## Formulas for DTU<sub>R</sub>

•

Probability of failure to perform while repair is onging  $(DTU_r)$  will depend on the operating philosophy. We assess different scenarios for illustration:

 $DTU_R \approx Pr(SIF \text{ is down due to a D failure})$ 

Pr(Remaining components have a hidden failure)

Three scenarios are presented with basis in a 2003 system:

 Scenario 1: A repair of a one D failure is ongoing. No change in configuration during repair, so the SIF is now a 2002 in this period. The DTU<sub>R</sub> becomes:

$$DTU_R \approx [3\lambda_D MTTR] \cdot [2 \cdot \frac{\lambda_{DU}\tau}{2}]$$

# Formulas for $DTU_R$ (cont.)

Three examples are presented with basis in a 2003 system (cont.):

- Scenario 2: One D failure is being repaired. The SIF is reconfigured to 1002 in this period. In this case, there is no contribution from  $DTU_R$  as the SIF now is more reliable than with 2003.
- Scenario 3: two failures are being repaired. The SIF is reconfigured to a 1001 system in this period. The DTU<sub>R</sub> becomes:

$$DTU_R \approx [(C_{2003} - C_{1003})\beta\lambda_{DU}MTTR] \cdot [\frac{\lambda_{DU}\tau}{2}]$$

The current version of the slide series do not include an explanation of  $DTU_T$ .

# P<sub>TIF</sub>

IF Probability of test independent failure,  $P_{T\!T\!F}$ : Unavailability due to test independent failures.

What do we mean by "test-independent failure"?

■ Test independent failure (TIF): A dangerous failure not revealed during a proof test.

- P<sub>TIF</sub> acknowledges that a proof test may not be perfect, and P<sub>TIF</sub> is a way to add a contribution fron this "imperfectness" of the test
- PDS method also suggest formulas using "proof test coverage" as an alternative.

### What is best? Proof test coverage or P<sub>TIF</sub>?

It is no general rule. What is important to evaluate if the regular testing has any impact at all. For example: The probability that a fire detector does not respond on demand due to wrong location may be independent of how often the fire detector is tested. Consequently, it may be argued that P<sub>TIF</sub> is most suited *in this specific case*.

Key Measures to Calculate

## Other Contributions of the PDS method

The PDS method covers a number of topics beyond formulas, for example:

- On failure classification
- Handing of systematic failures
- Analysis of multiple SIFs

Visit the PDS method for more information.