# Stress sensitivity of non-elastic processes in a weak sandstone

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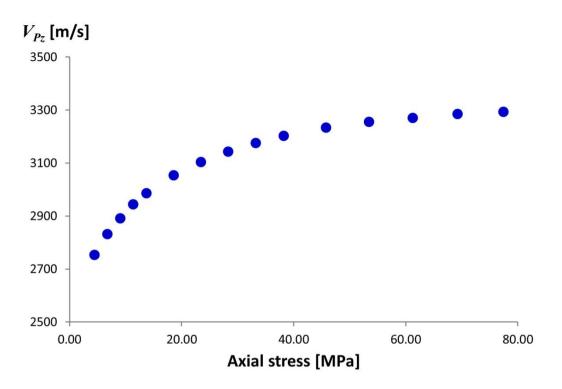






Wave velocities of soft rocks depend on stress.

## Why?



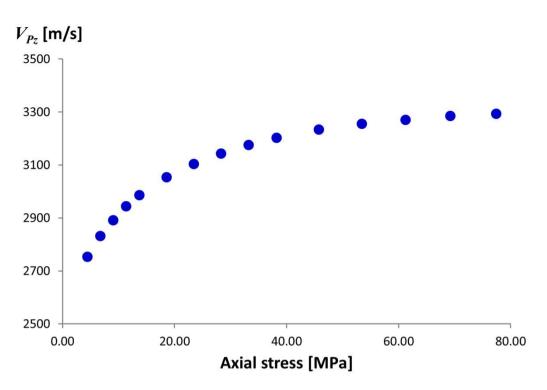
Wave velocities of soft rocks depend on stress.

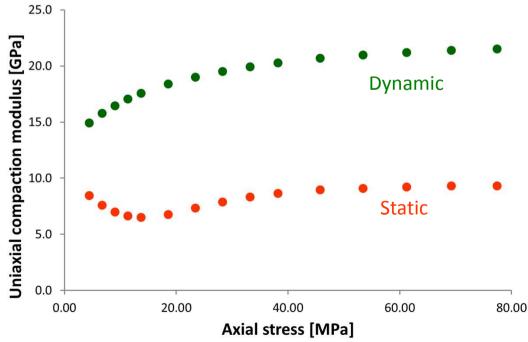
#### Why?

Static and dynamic moduli of soft rocks are different - also for dry rocks.

The difference changes along the stress path.

#### Why?





# Potential processes causing non-linear elastic and non-elastic behavior



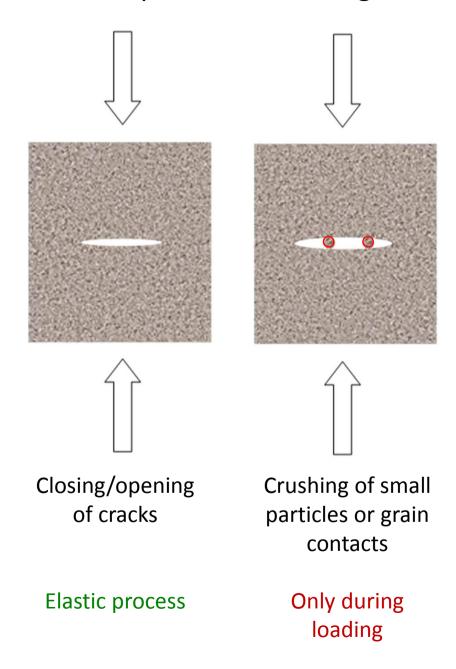




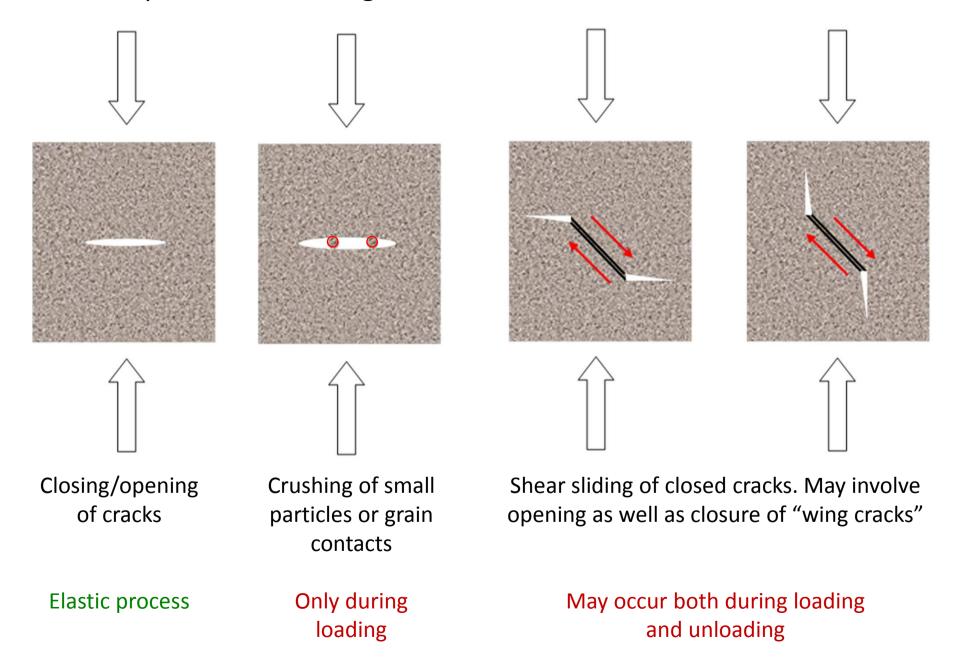
Closing/opening of cracks

Elastic process

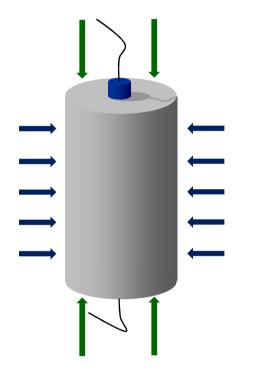
## Potential processes causing non-linear elastic and non-elastic behavior



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#### Laboratory tests:



# Standard triaxial set-up + acoustics

**Axial stress** 

Confining stress

Axial wave propagation

- P-waves
- S-waves

#### Here:

- Dry outcrop sandstone → No fluid effects
- Castlegate sandstone → No clay effects
- KO path  $\rightarrow$  Both static and dynamic  $C_{33}$
- Unloading → Exclude crushing of contacts

## Static vs dynamic:

#### Non-elastic compliance:

$$S_{H} = \frac{1}{C_{33}^{st}} - \frac{1}{C_{33}^{el}}$$

$$C_{33}^{st} = \frac{\Delta \sigma_{z}}{\Delta \varepsilon_{z}} \text{ (static)}$$

$$C_{33}^{el} = \rho V_{P,z}^{2} \text{ (dynamic)}$$

$$Start \text{ unloading}$$

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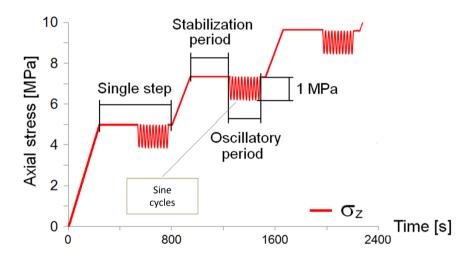
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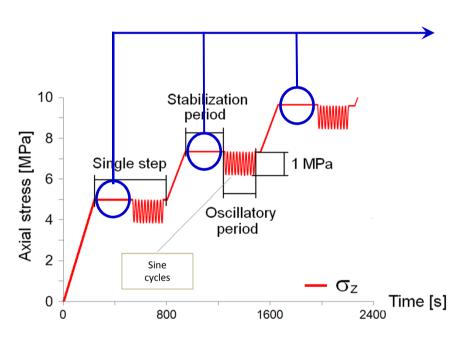
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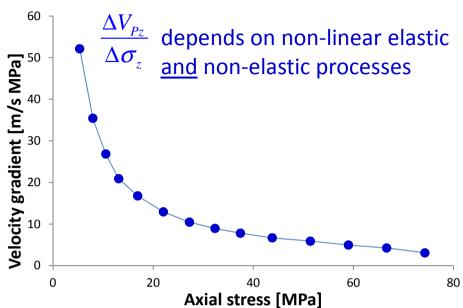
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# Non-linear acoustic tests (Stroisz and Fjær, 2011):

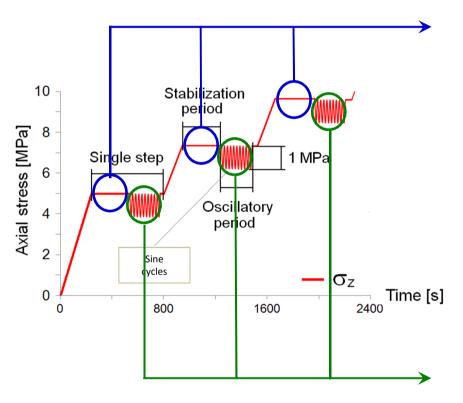


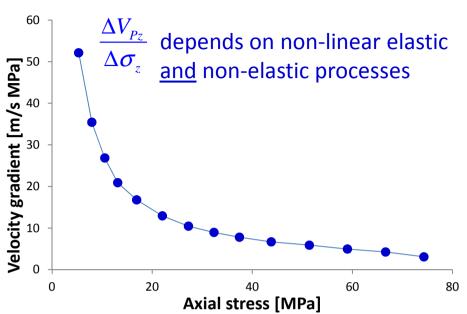
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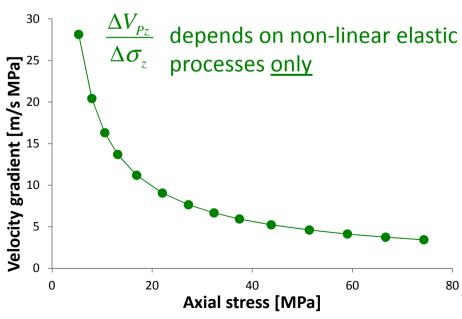




# Non-linear acoustic tests (Stroisz and Fjær, 2011):







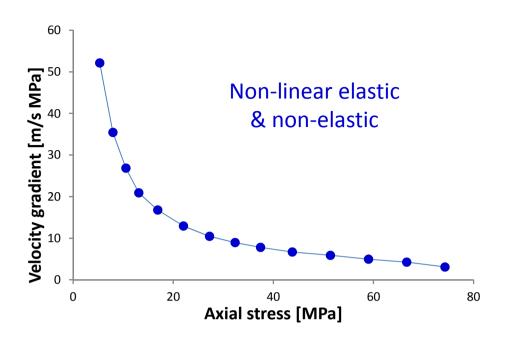
Non-linear elastic & non-elastic

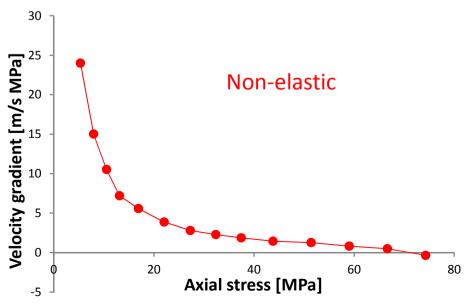
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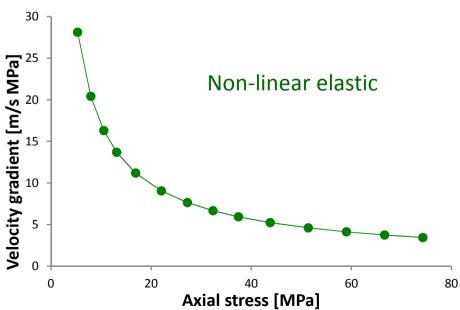
Non-linear elastic

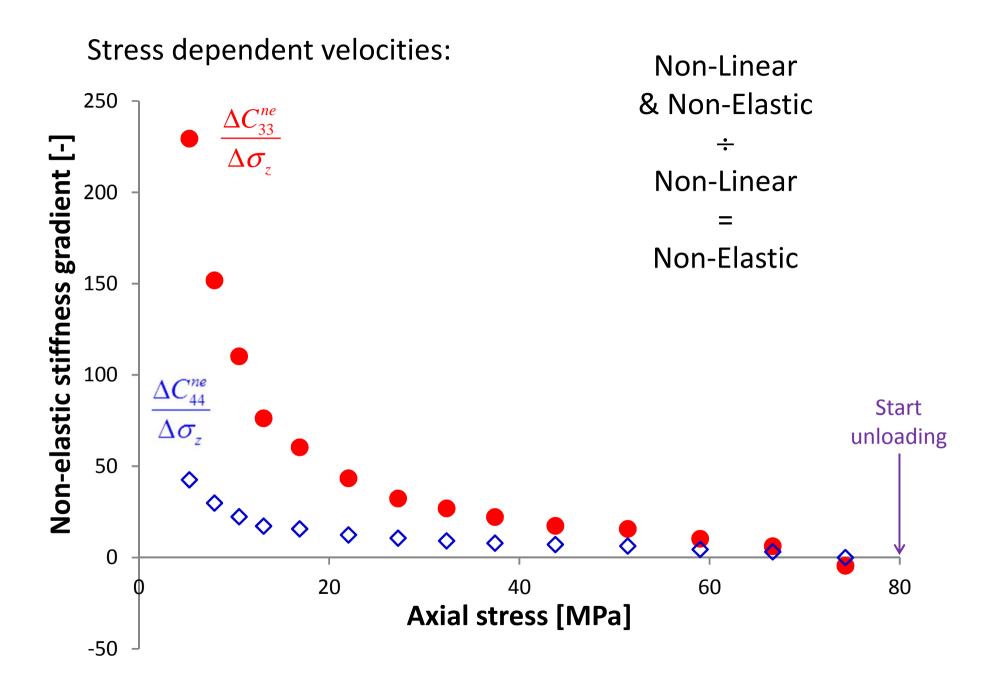
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Non-elastic



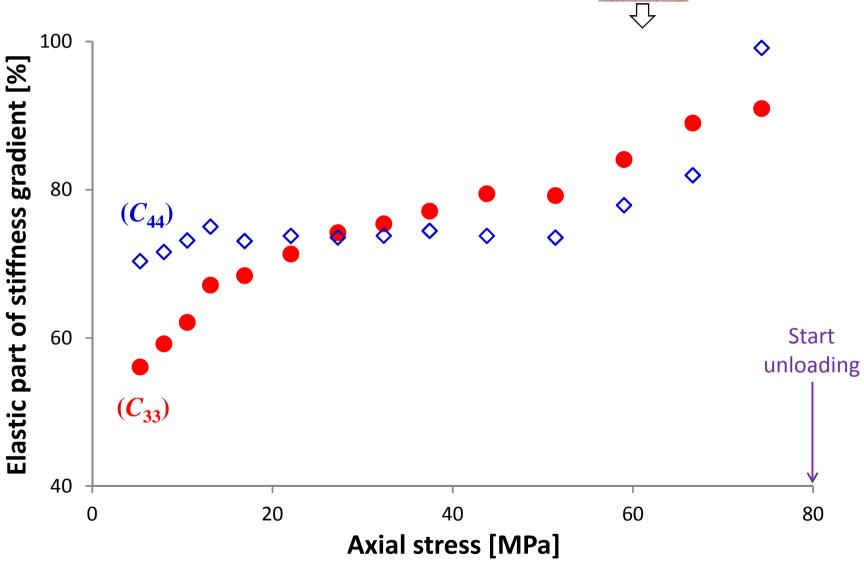






The stress dependence of wave velocities is mostly due an elastic process





#### Stress dependent velocities:

Non-elastic part of stiffness gradient

$$\frac{\Delta C_{33}^{ne}}{\Delta \sigma_{_{_{Z}}}}$$

#### Static vs dynamic:

Non-elastic compliance

$$S_H = \frac{1}{C_{33}^{st}} - \frac{1}{C_{33}^{el}}$$

#### Stress dependent velocities:

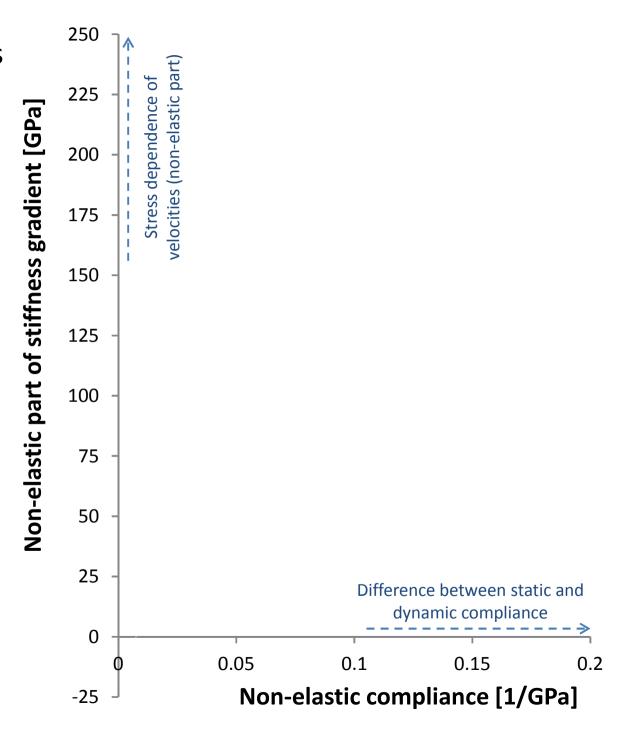
Non-elastic part of stiffness gradient

$$\frac{\Delta C_{33}^{ne}}{\Delta \sigma_{z}}$$

Static vs dynamic:

Non-elastic compliance

$$S_H = \frac{1}{C_{33}^{st}} - \frac{1}{C_{33}^{el}}$$

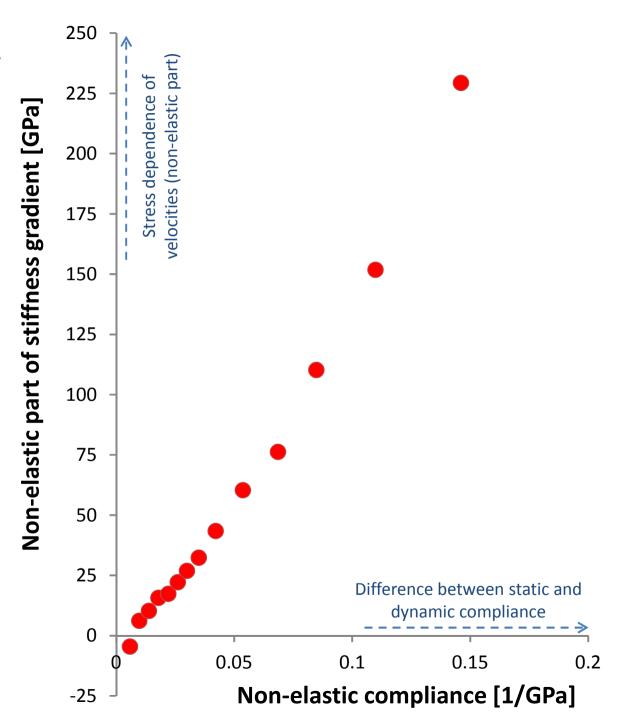


Stress dependent velocities: Non-elastic part of stiffness gradient

 $rac{\Delta C_{33}^{ne}}{\Delta oldsymbol{\sigma}_z}$ 

Static vs dynamic: Non-elastic compliance

$$S_H = \frac{1}{C_{33}^{st}} - \frac{1}{C_{33}^{el}}$$



# <u>Stress dependent velocities</u>:

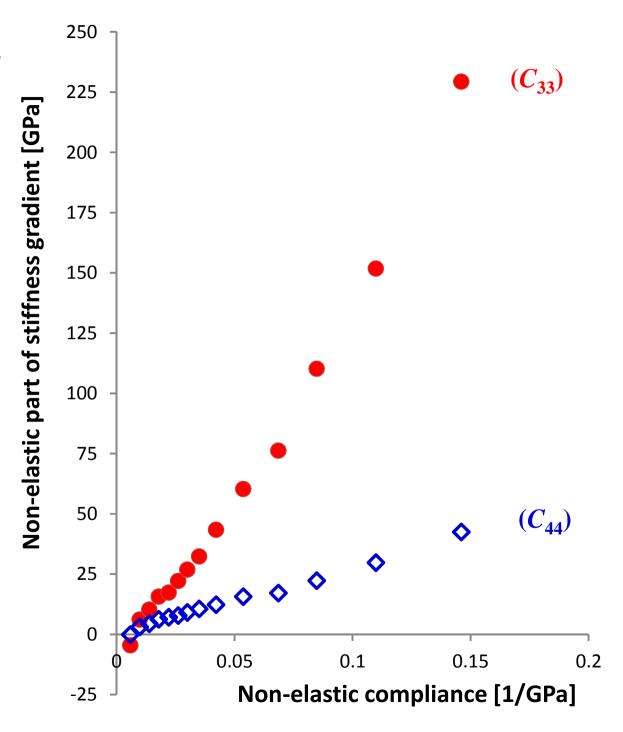
Non-elastic part of stiffness gradient

$$rac{\Delta C_{33}^{ne}}{\Delta oldsymbol{\sigma}_z}$$

#### Static vs dynamic:

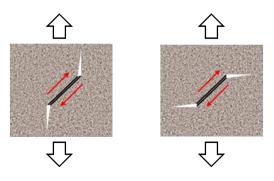
Non-elastic compliance

$$S_H = \frac{1}{C_{33}^{st}} - \frac{1}{C_{33}^{el}}$$

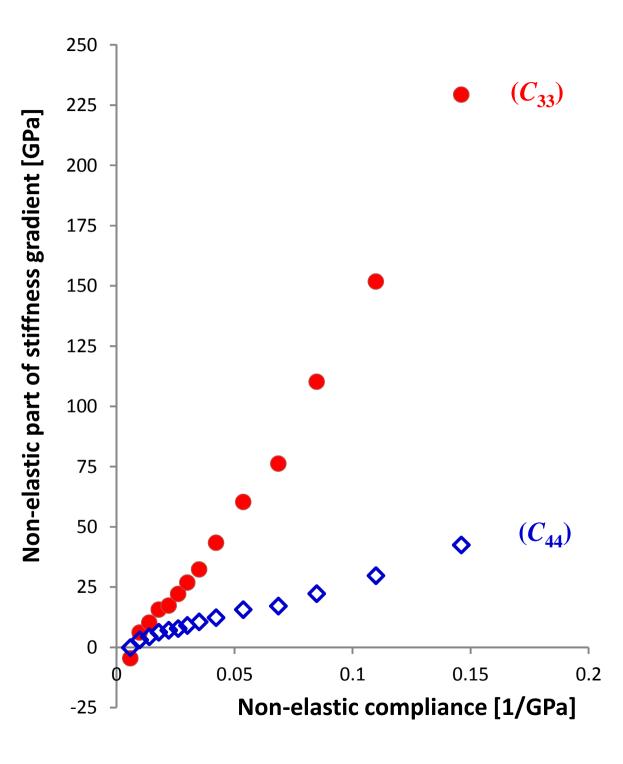


Very clear correlation
between
the non-elastic part of the
stiffness gradient
and
the non-elastic compliance

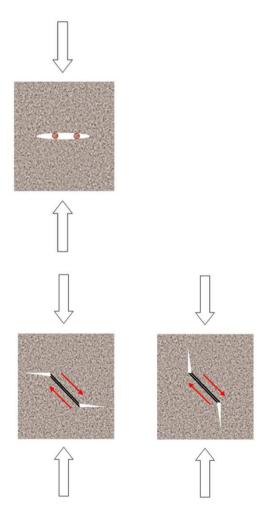
Suggests that the same process controls both parameters during unloading

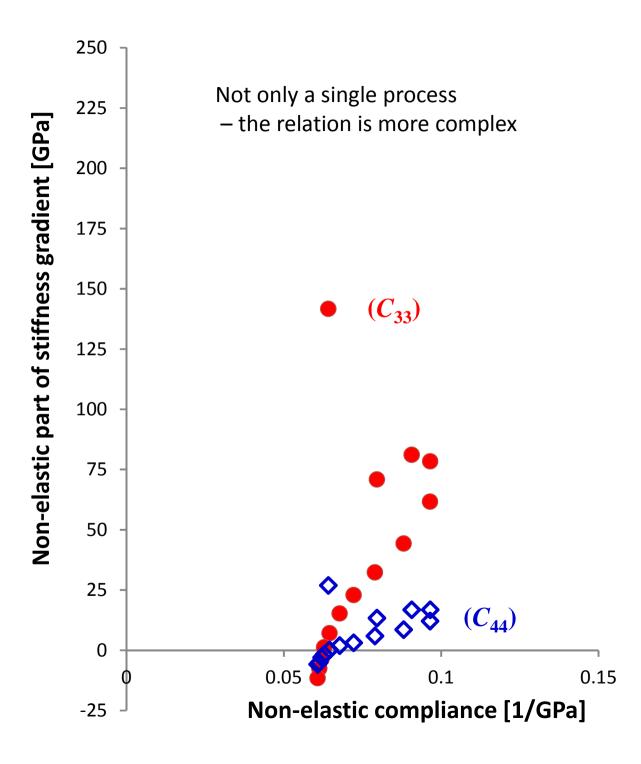


Shear sliding of closed cracks



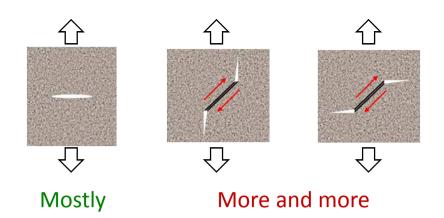
During **loading**, also crushing of small particles or grain contacts will occur

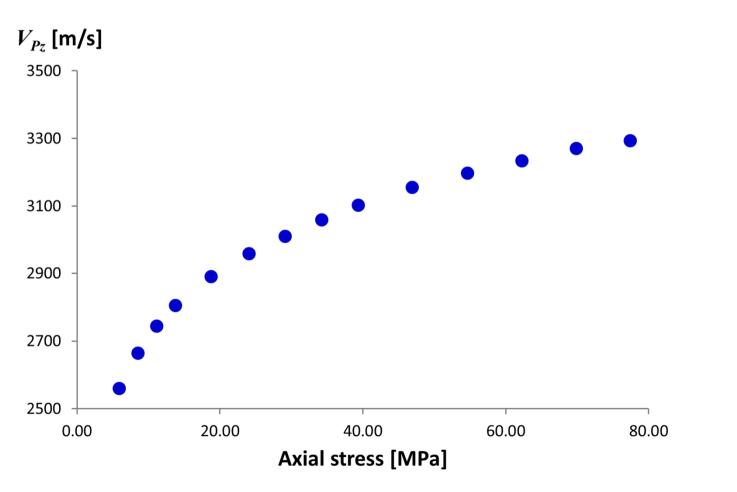




#### **KO** unloading of a dry, clay-free sandstone:

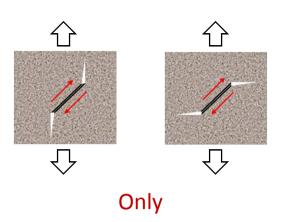
Wave velocities of soft rocks depend on stress - because:

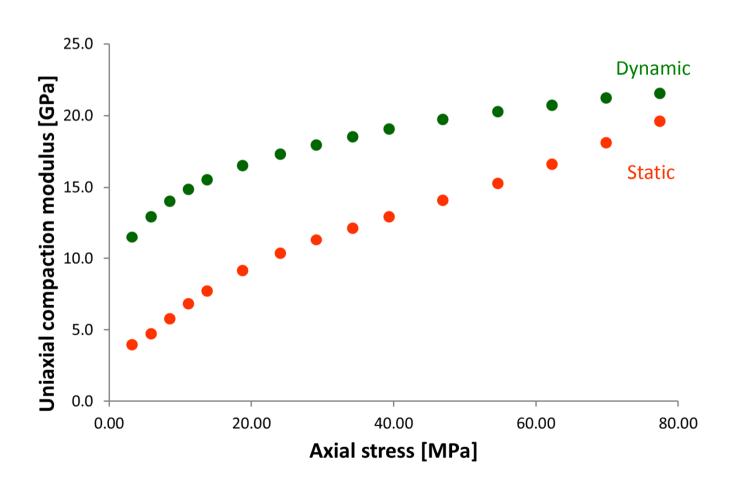




#### **KO** unloading of a dry, clay-free sandstone:

Static and dynamic moduli of soft rocks are different - because:





#### **Summary:**

- During KO unloading of a dry, clay-free sandstone, the stress dependence of elastic waves is mainly caused by an elastic process, but a non-elastic process causing opening/closure of cracks become increasingly important
- The same non-elastic process appears to be the cause for the difference between static and dynamic moduli under these conditions
- This non-elastic process may be associated with shear sliding of closed cracks

#### **Acknowledgements**

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- Petrobras, through Rede de Technologia de Poços (CENPES)