# Dynamic Testing of Distance Protection according to IEC 60255-121 Standard

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## **Presentation Summary**

- Research Objectives
- Dynamic Performance of Distance Protection
- Test Methodology
- Results and Analysis
- Conclusions



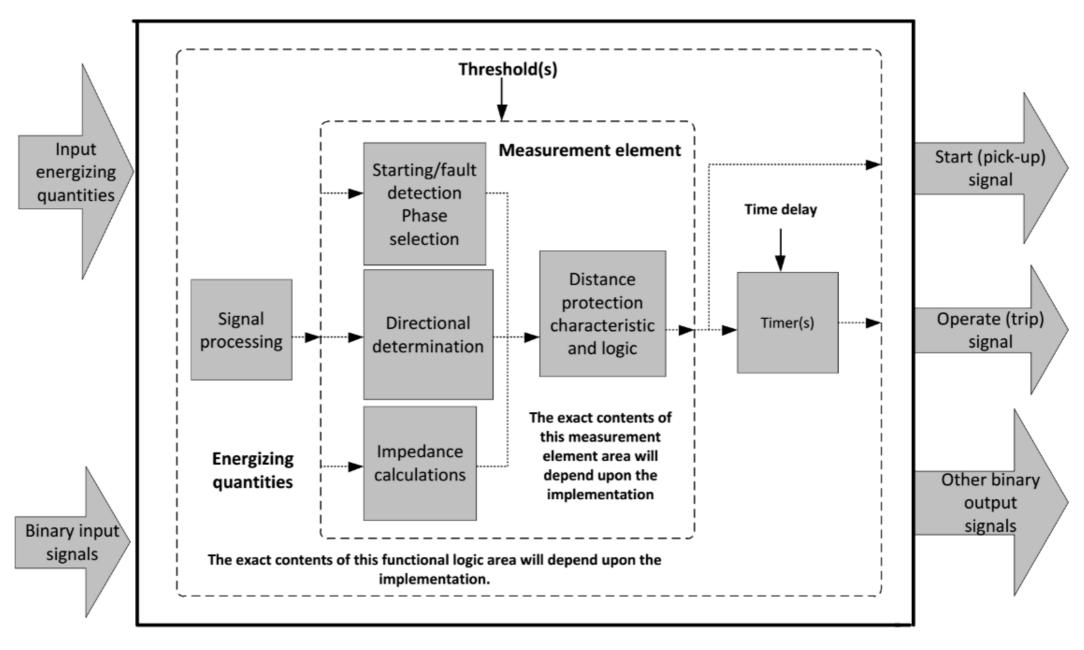
## Research Objective

 To develop distance protection test modules according to IEC 60255-121:2014 using ATP/EMTP and OMICRON Control Center

+ To analyze the distance protection relay performance against dynamic conditions



## Dynamic Performance of Distance Protection





Simplified distance protection function block (IEC 60255-121)

- The dynamic performance is the response of distance protection function to various power system conditions (such as faults)
- It provides a complete assessment of all distance relay functions:
  - Signal processing block
  - Starting/fault detection algorithm
  - Directional determination algorithm
  - Impedance calculation algorithm
  - Protection characteristic and logic
- Dynamic performance is defined in terms of operating time and reach accuracy
  - Operating time is the time interval between the instant when fault occurs and the instant when relay operates (trip)
  - Reach accuracy means no overreach or underreach operation under all dynamic condition



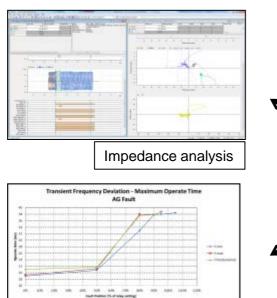
# Dynamic performance test according to IEC 60255-121:2014

- The standard includes methods to test and verify the operating time and reach accuracy of Zone-1 under dynamic conditions
- It requires proper transient simulation tools, and testing equipment in order to executed the test cases
- Dynamic conditions covered in this research:
  - + Effects of Capacitive Voltage Transformer (CVT) transient
  - + Performance with harmonics
  - + Performance with frequency deviation
  - + Performance under fault with resistance and pre-fault load
  - + Performance under dynamic fault (evolving faults and current reversal condition)

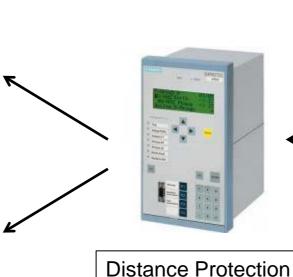


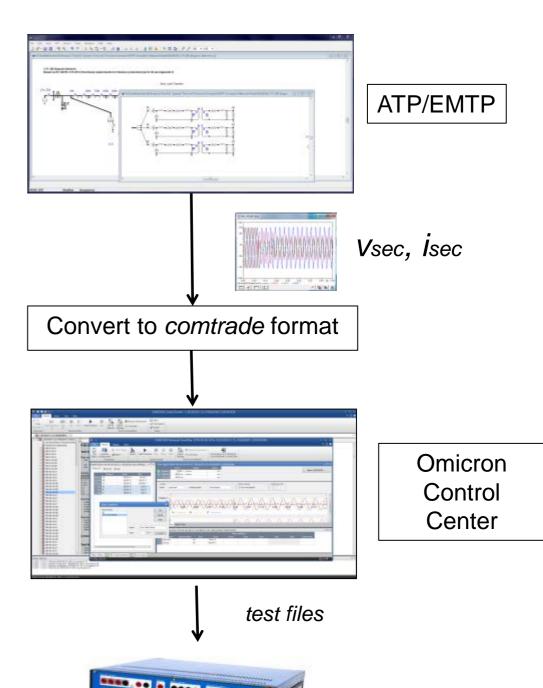
## Test Methodology

- Transient Simulation using ATP/EMTP
  - + Network & Components Modelling
  - + Fault Test Cases Simulation
  - + Recording of Transient Waveform
- Test set-up
  - + Omicron CMC 356
  - Numerical Distance Protection
    - + Relay M
    - + Relay N
- Result analysis



SIR Diagram





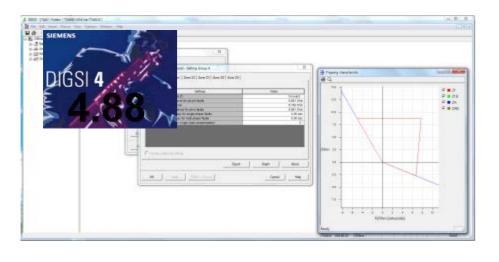


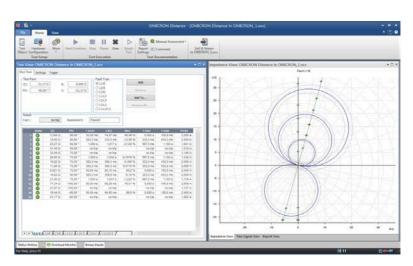
### Test Set-Up

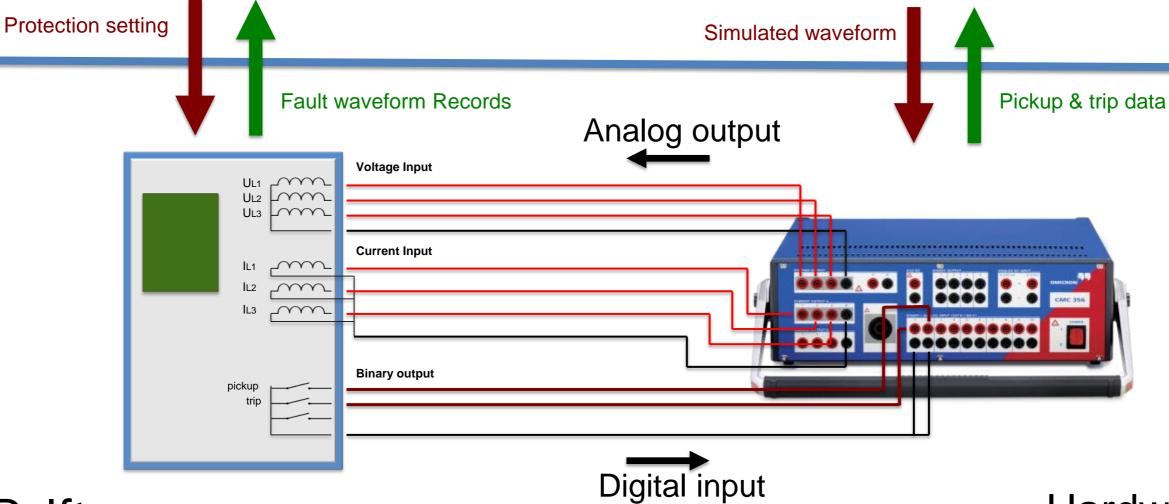
#### Software

Relay Software Interface

**Omicron Control Center** 





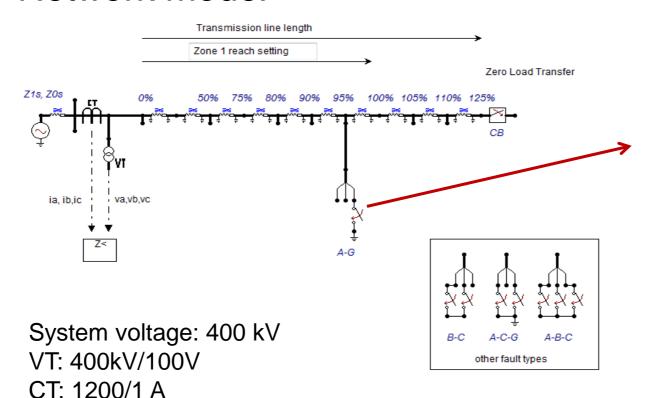




Hardware

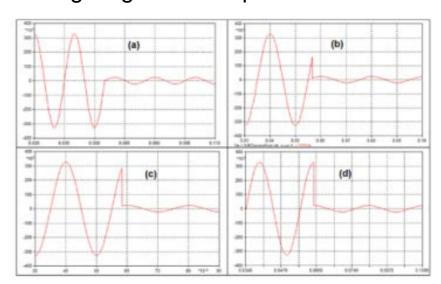
# Distance protection performance with different dc-offset, faulted phases, and source impedance ratio (SIR)

#### Network model



Zone 1 setting: 80% transmission length

Fault inception angle: the angle between the inception of the fault and the nearest preceding zero crossing of voltage signal with a positive derivative



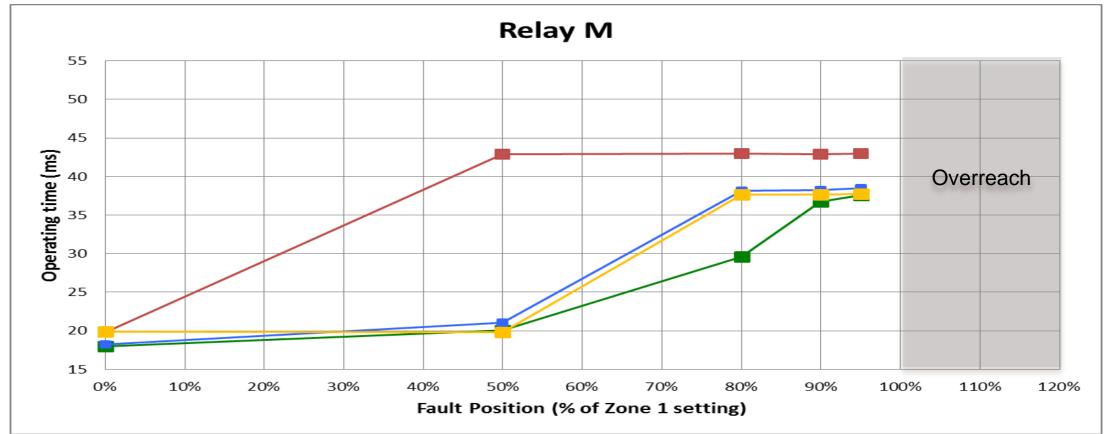
Fault inception angle for L-N fault (a) 0°, (b) 30°, (c) 60°, and (d) 90°

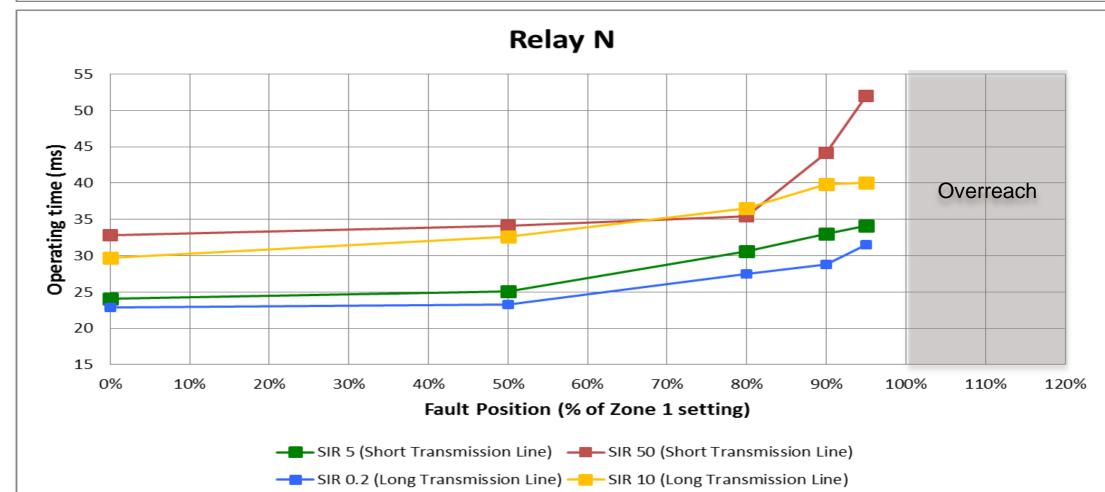
#### Test cases (total 448 test cases and 1792 test shots)

Line model	Source impedance ratio (SIR)	Fault position (% of Zone 1 setting)	Fault type	Fault inception angle (°)
Short transmission line (20 km)	5 and 50	0, 50, 80, 90, 95, 105, and 110	A-G, B-C, B-C-G, and A-B-C	0, 30, 60, 90
Long transmission line (100 km)	0.2 and 10	0, 50, 80, 90, 95, 105, and 110	B-G, A-C, A-C-G, and A-B-C	0, 30, 60, 90



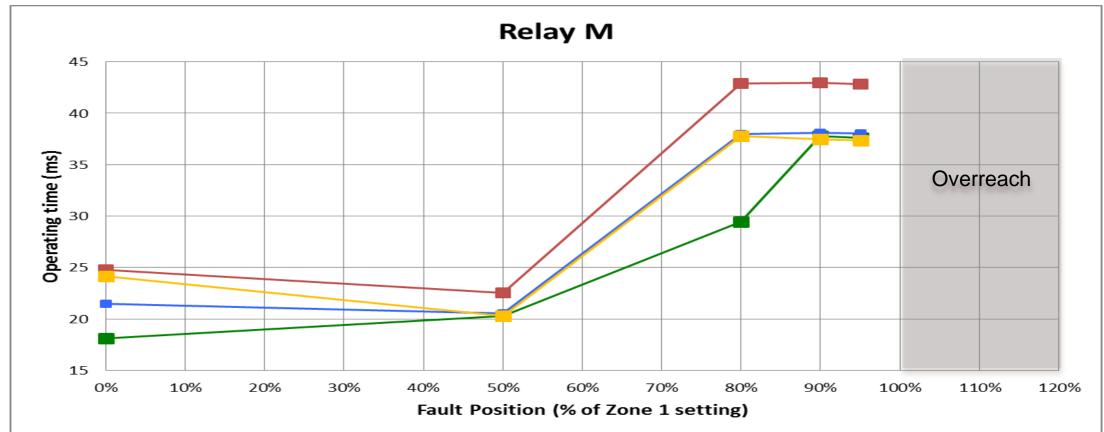
#### Average operating time for L-N fault

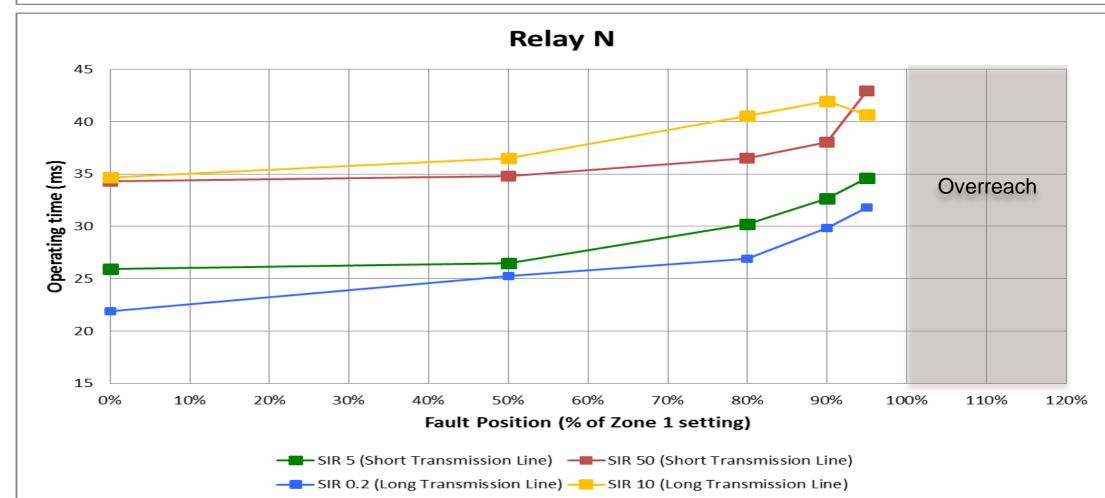






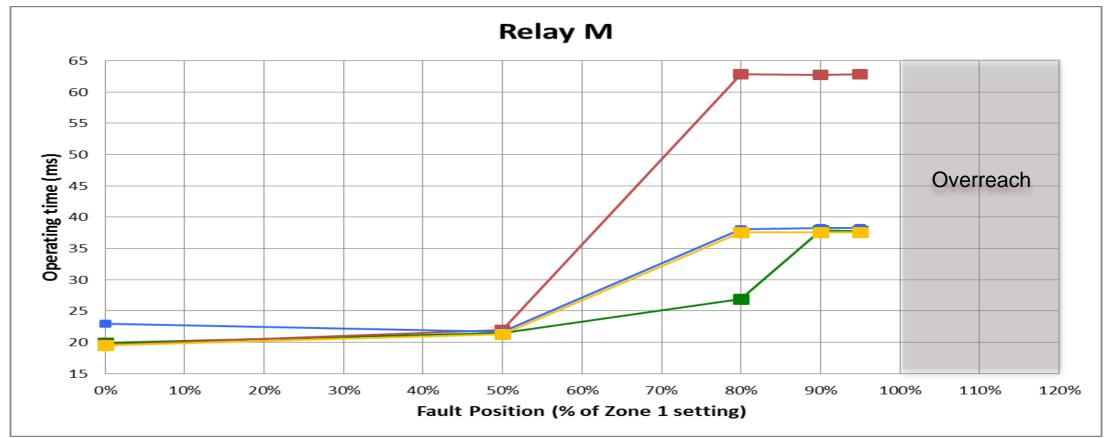
#### Average operating time for L-L fault

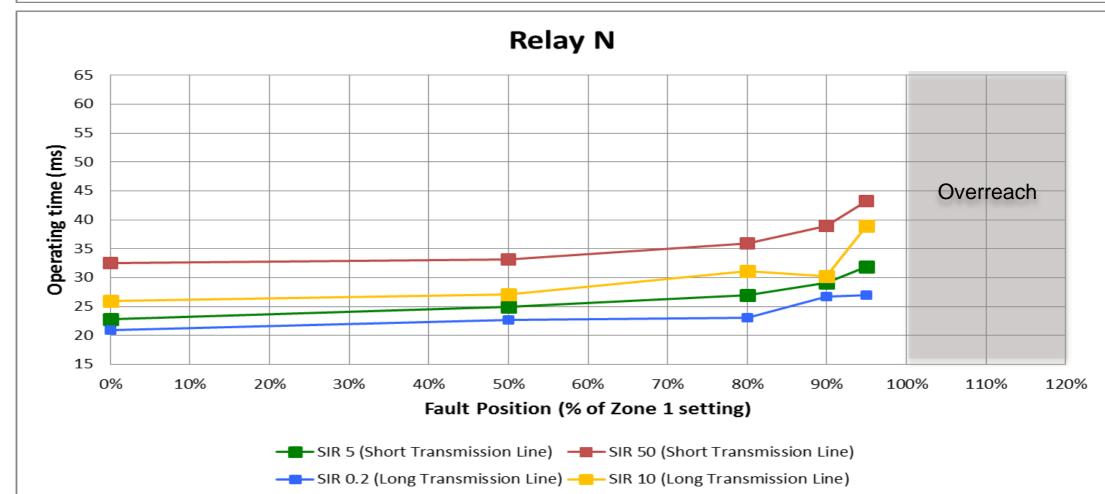






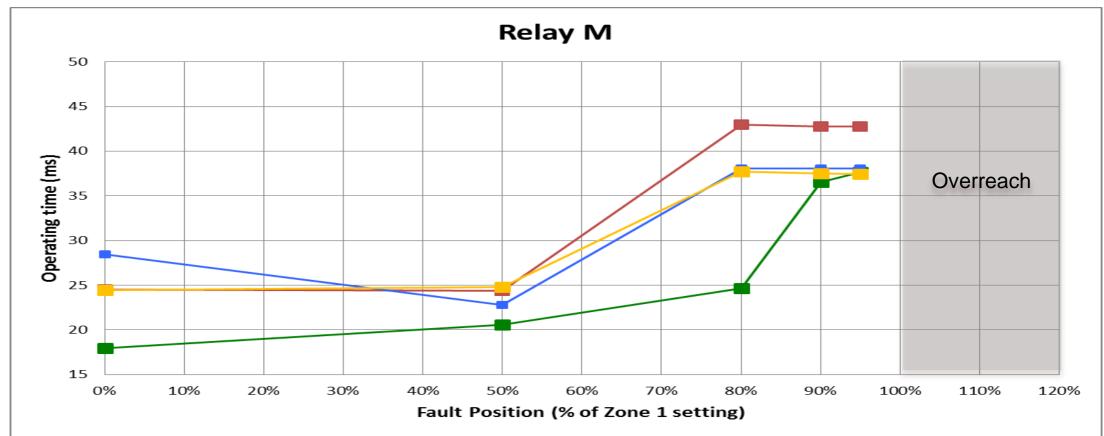
#### Average operating time for L-L-N fault

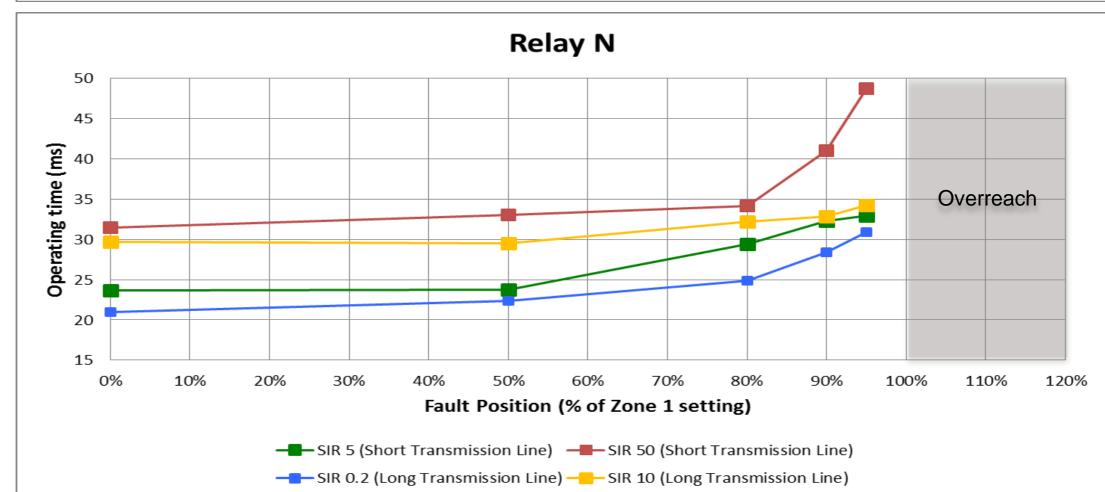






#### Average operating time for L-L-L fault

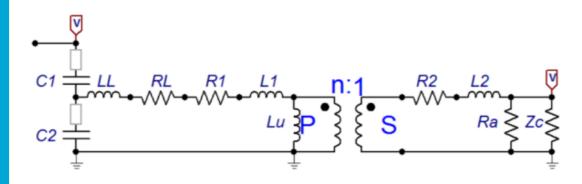






# Distance protection performance with CVT transient

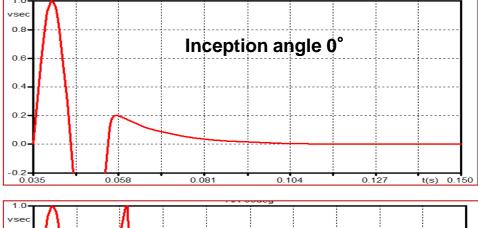
#### CVT model

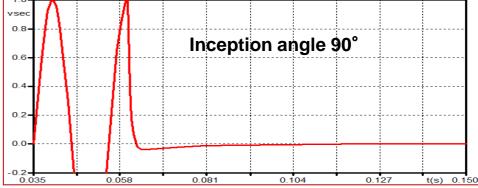


Vpri	400000	V	Ra	177700	Ω
Vsec	100	V	LL	107	H
C1	4210	pF	L1	5	H
C2	80000	pF	L2	8	H
Ce	0	pF	Lμ	177820	H
RL	650	Ω	Zc	80/1840	VA/ kΩ
R1	1550	Ω	Load PF	1	
R2	2700	Ω			

**CVT Parameter (IEC 60255-121)** 

#### Transient response of the model

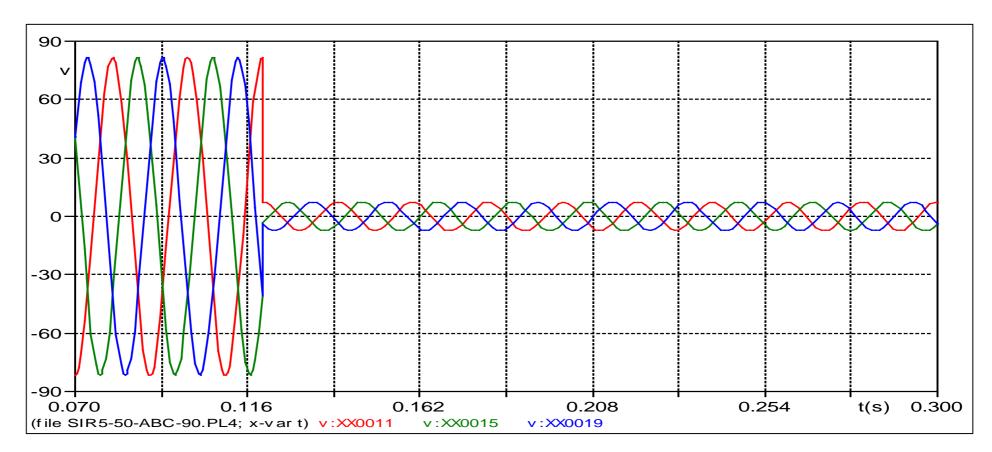




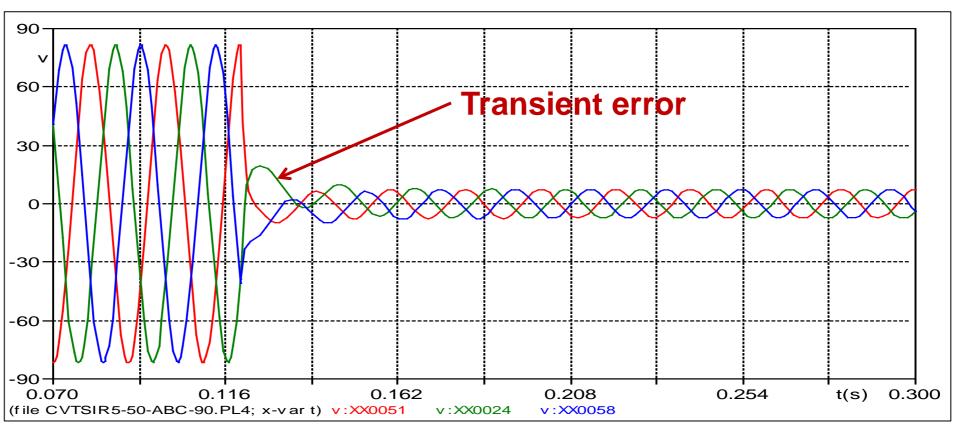
#### Test cases (total 224 test cases and 896 test shots)

Line model Source impedance ratio (SIR)		Fault position (% of Zone 1 setting)	Fault type	Fault inception angle (°)
Short transmission line (20 km)	5 and 50	0, 50, 80, 90, 95, 105, and 110	A-G, B-C, A-C-G, and A-B-C	0, 30, 60, 90





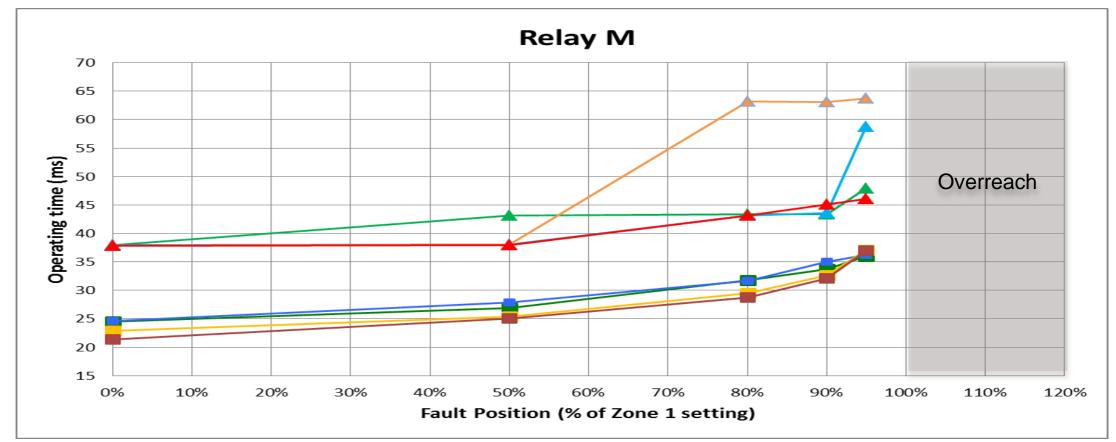
VT secondary voltage for A-B-C fault at 95% of zone 1

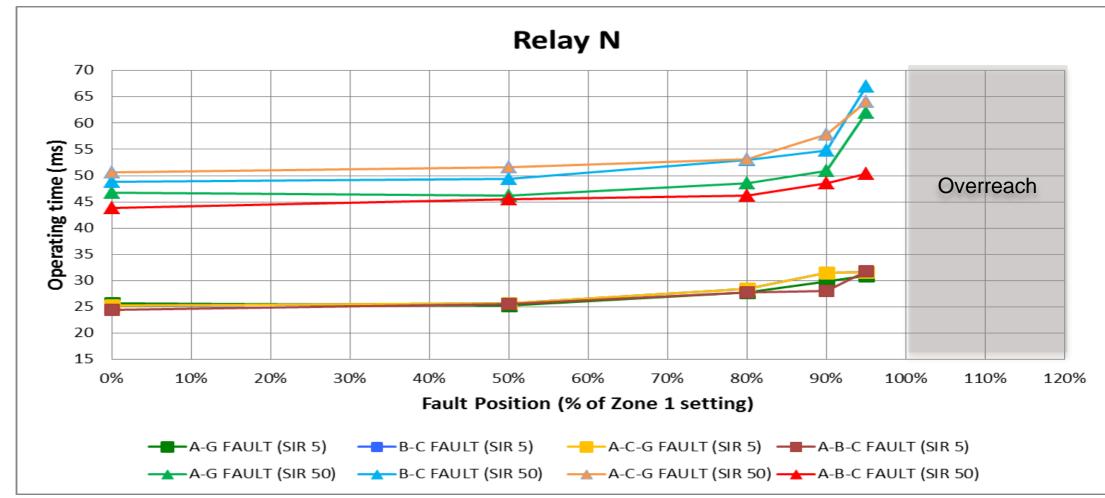


CVT secondary voltage for A-B-C fault at 95% of zone 1



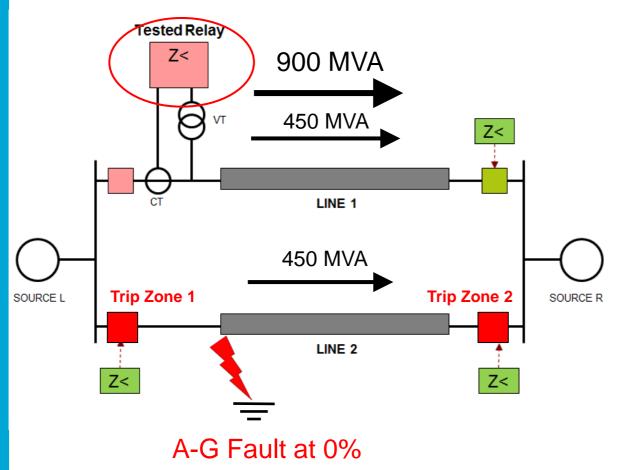
#### Average operating time with CVT







# Distance protection performance with current reversal



#### **Simulation Sequence in ATP/EMTP**

- 1. Pre-fault export load 450 MVA for each line
- 2. Fault occurs on line 2, seen in reverse direction by tested relay
- 3. Correct trip of zone 1 after 60 ms
- 4. Correct trip of zone 2 after 300 ms
- 5. Double export load flow 900 MVA on line 1

The tested relay is expected NOT to trip in forward direction

#### Test result

Fault	Fault Type	Fault on line	Fault position	Zone 1	Operatino	g Time (ms)
no.	i auit on line	i auit position	Criteria	RELAY M	RELAY N	
89	A-G	2	+0%	No Trip	-	-



#### Conclusions

- Modules for dynamic testing of distance protection according to IEC 60255-121 have been developed using ATP/EMTP simulation and Omicron tester
- Dynamic performance comparisons of distance relay M and N are as follow:
  - The operating time of relay M is faster than relay N in case of near busbar faults.
    While for end of zone-1 faults, relay N operate faster than relay M.
    - + Close in faults: Relay M: 24.4 ms; Relay N: 31.1 ms
    - + End of Zone-1 faults: Relay M: 41.9 ms and Relay N: 36 ms
  - The average tripping delays caused by:
    - + High SIR: Relay M: 8.5 ms; Relay N: 6.9 ms
    - + CVT transient in high SIR: Relay M: 6.9 ms and Relay N: 14.1 ms
  - Both distance protections seem to have problems to detect faults with resistance. Relay M and relay N fails to trip 17 times and 5 times from the total 88 test cases, respectively. Furthermore, most of the fails-to-trip cases occur on short transmission lines (21 out of 22 cases)



#### Conclusions

- Dynamic performance of relay M against harmonics, frequency deviation, and evolving faults can be summarized as follow:
  - Certain harmonics order could cause severe delay in its operating time, in this case 7<sup>th</sup> harmonics caused delay up to 18 ms for AG fault at 95% of zone 1 setting
  - Frequency deviation does not affect its operating time. However, the relay seems to have overreach problems when operating on minimum frequency
  - The Relay shows good selectivity function for evolving faults

