

Flexible Risers with Slug Flow

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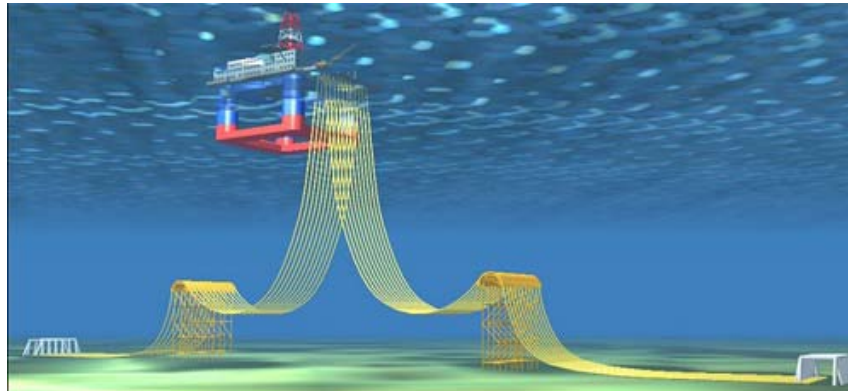
Retirement of Prof. Carl M. Larsen

Trondheim, August 21, 2015

Flexible Risers with Slug Flow

Objective:

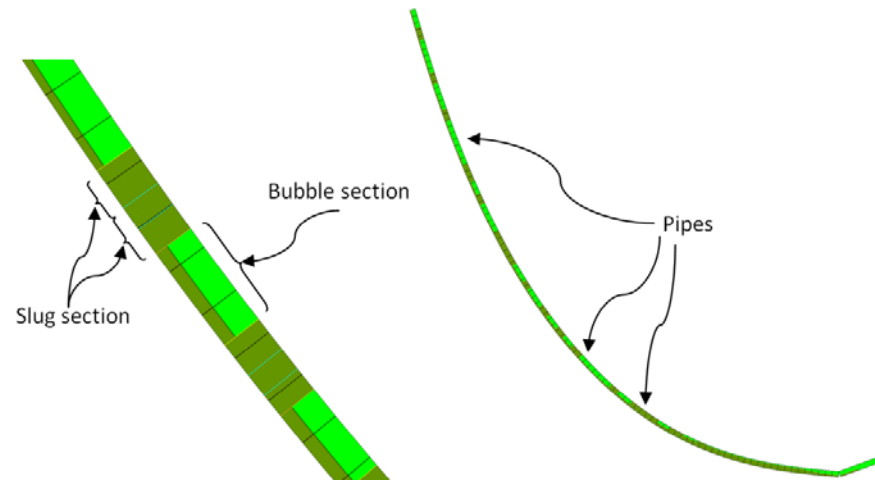
1. Influence of slug flow in dynamic response of flexible risers.
2. Influence of the dynamic riser configuration in development of slug flow.
3. Build a computational tool for simulation of the fluid-structure interaction.



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Slug Flow Program:

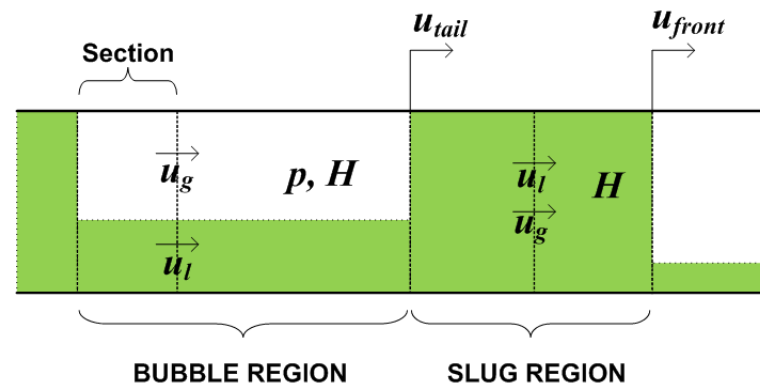
- Program for simulation of unsteady slug flow in pipes and risers.
- *In-house* code.
- OOP, written C++.
- Based on a Lagrangian Slug Tracking Model.



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Slug Flow Program:

- Slugs and bubbles are considered as objects.
- Objects have characteristic data (holdup, velocities, and pressure)
- Fluid conservations equations are balanced into each object.
- Similarly slugs and bubbles are linked by mass and momentum balances



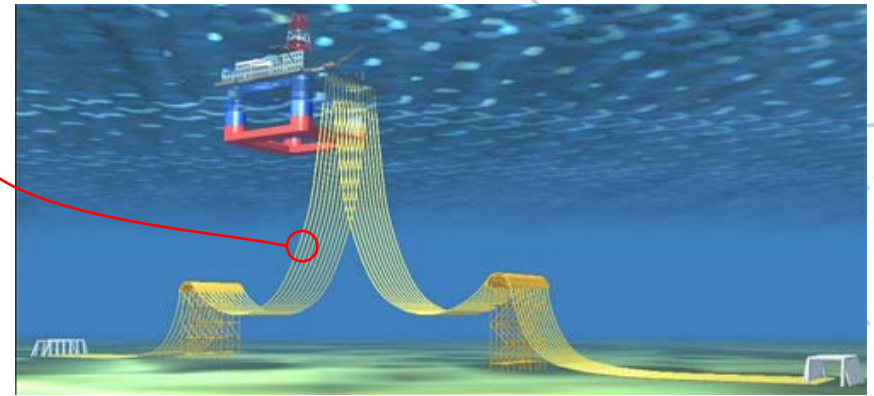
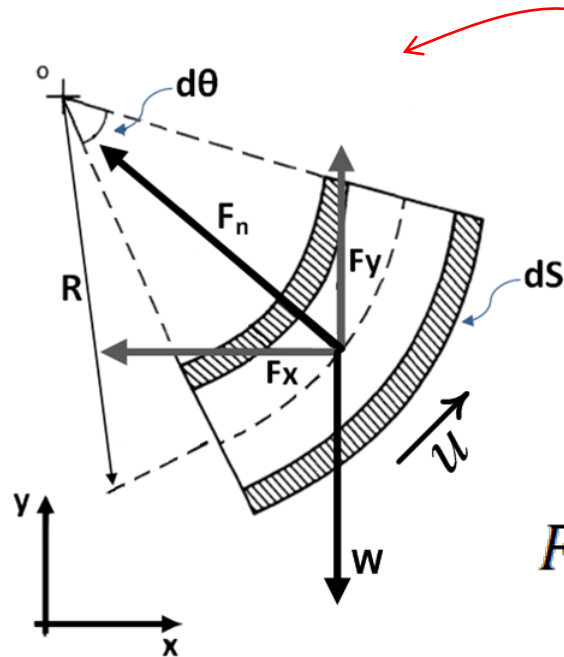
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Riser Analysis Program:

- Program for GRA of flexible risers.
- *In-house* code.
- Modular programming written in Fortran.
- Static and dynamic analysis.
- Lazy-wave, catenary and other arbitrary riser configurations.
- Simulate forces from waves and internal single/two-phase flow.
- Based in a non-linear FEM.

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A fluid particle traveling along a riser:



F_n : normal equivalent force / centripetal force

- From the conservation equations:

$$F_n = \rho_{\text{fluid particle}} A U_{\text{fluid particle}}^2 \frac{dS}{R}$$

- For two-phase flow:

$$F_n = F_{n_l} + F_{n_g} \quad F_{n_k} = M_k \frac{U_k^2}{R}$$

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Incremental formulation of Dynamic Equilibrium Equation:

$$M^* \Delta \ddot{r} + C \Delta \dot{r} + K \Delta r = F^{e*} - F^{i*}$$

* Variation due to two-phase flow:

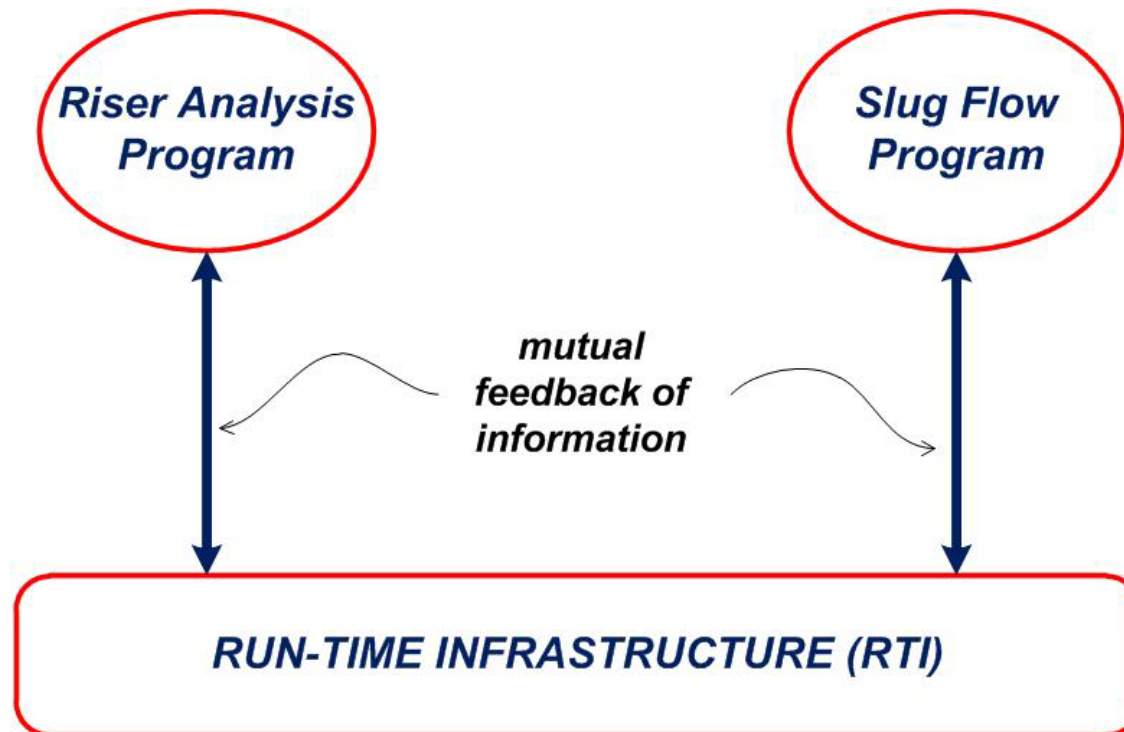
$$M^* = M_{pipe} + M_{added} + M_l + M_g \quad \text{mass matrix}$$

$$\vec{F}^{e*} = \sum \vec{F}^e + M_l (\vec{a}_{c_l} + \vec{g}) + M_g (\vec{a}_{c_g} + \vec{g}) \quad \text{external force vector}$$

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Communication Interface:

Independent but Interconnected Systems.



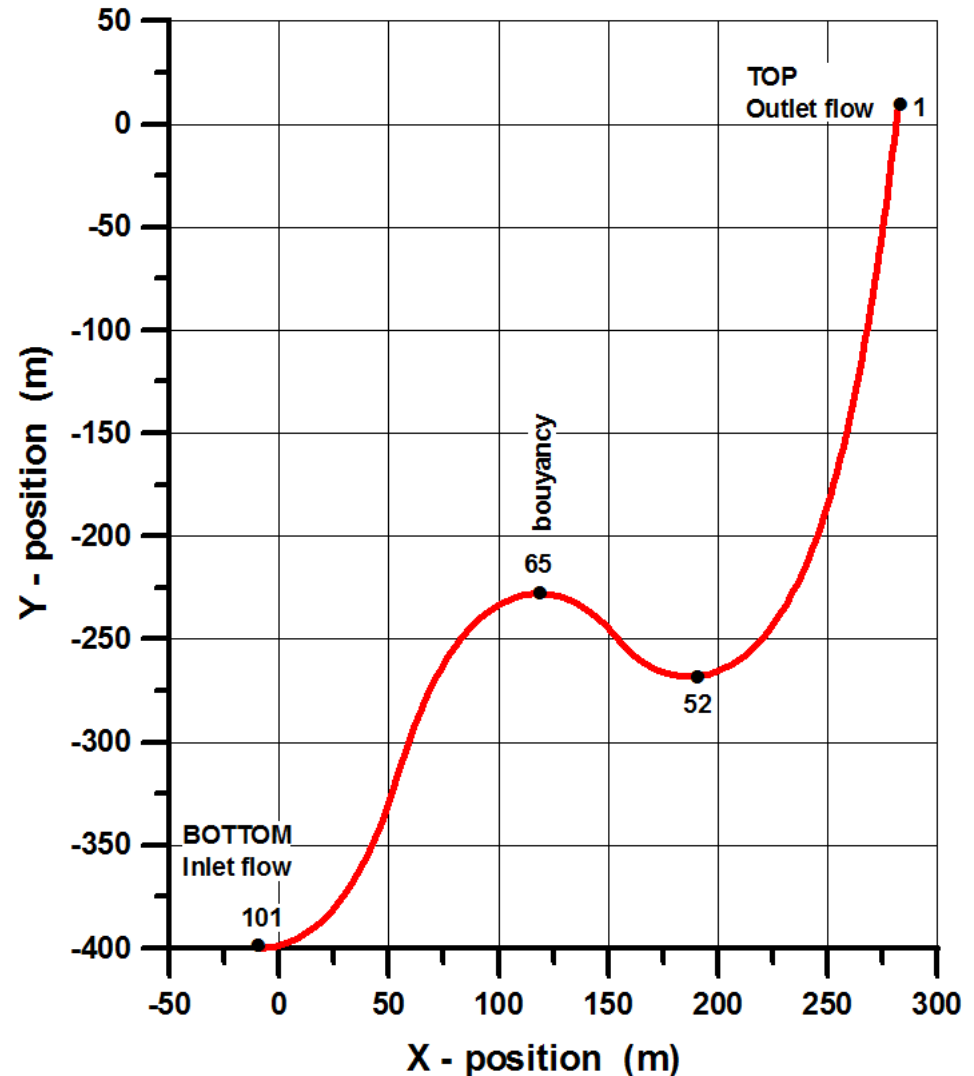
High Level Architecture (HLA)

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Case Base 1:

- Lazy-wave configuration.
- Water depth: 400 m
- Riser length: 620 m
- External diameter: 0.4 m
- Discretization: 100 elements
- Inlet liquid flow rate: 300 kg/s
- Inlet gas flow rate: 8 kg/s
- Outlet pressure: 1 atm.
- Hydrodynamic slugging.

Snap-shot of riser shape after static analysis

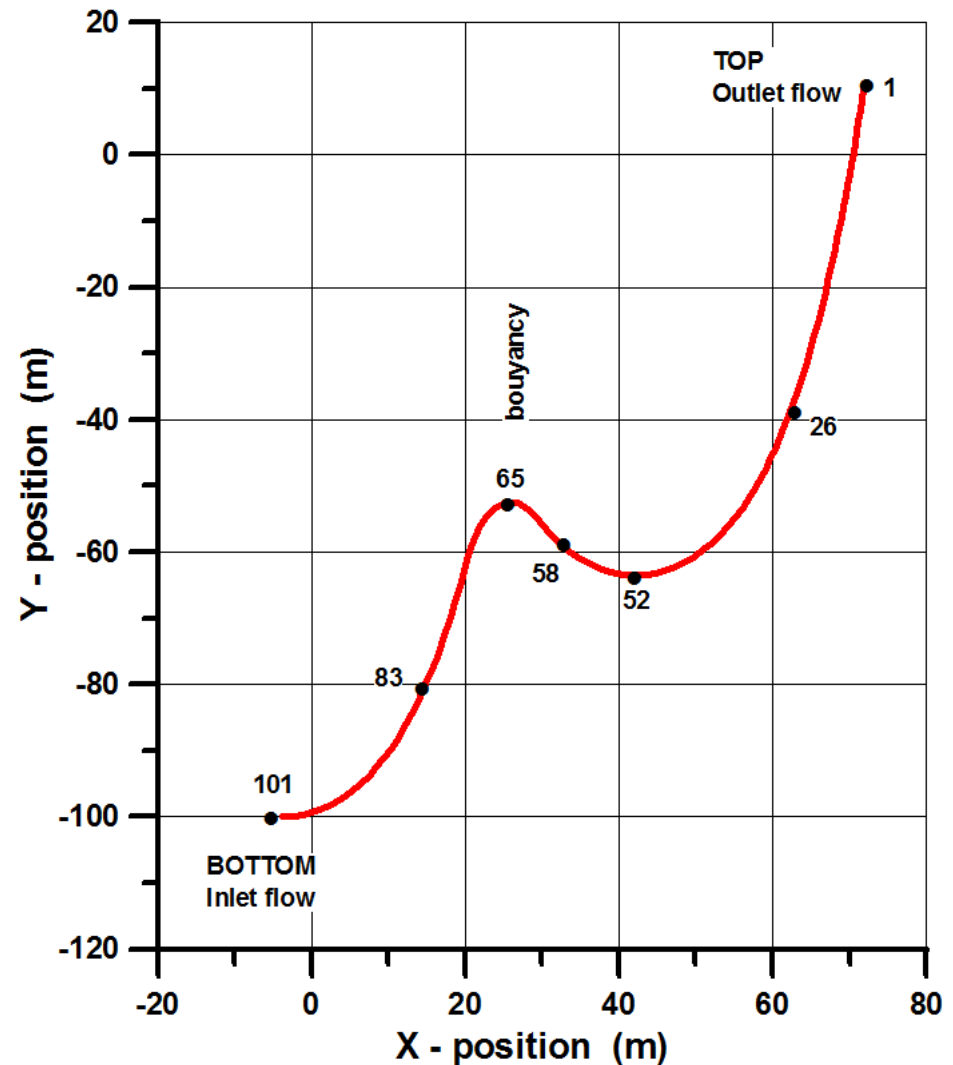


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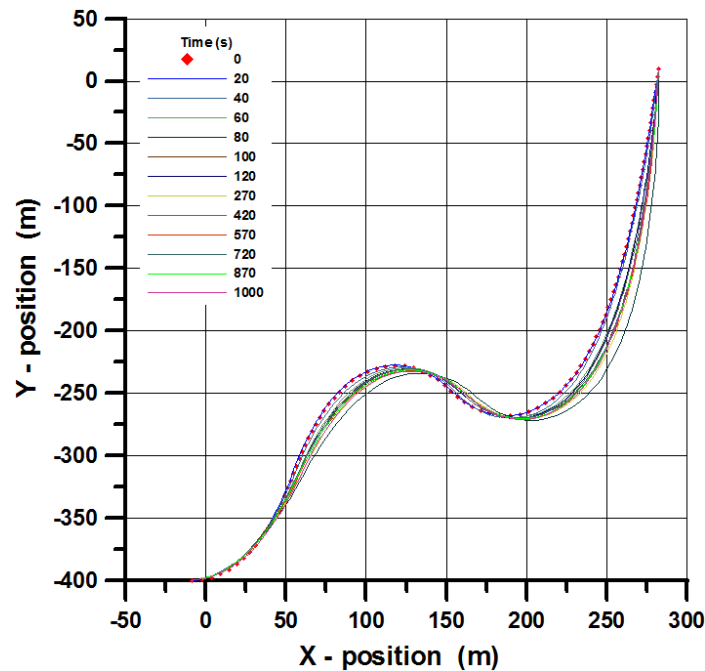
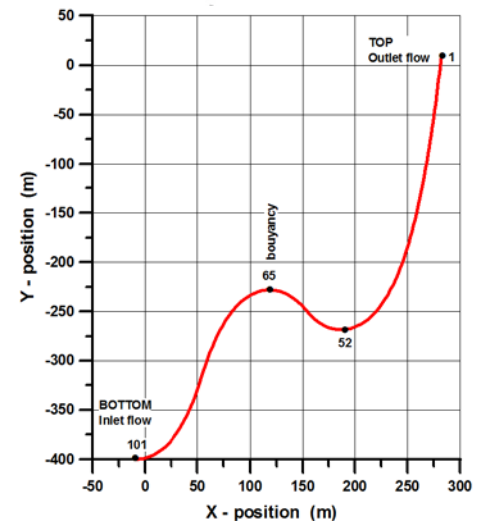
Case Base 2:

- Lazy-wave configuration.
- Water depth: 100 m
- Riser length: 160 m
- Internal diameter: 6 in
- Discretization: 100 elements
- Inlet liquid flow rate: 9 kg/s
- Inlet gas flow rate: 0.25 kg/s
- Outlet pressure: 1 atm.
- Severe slugging.

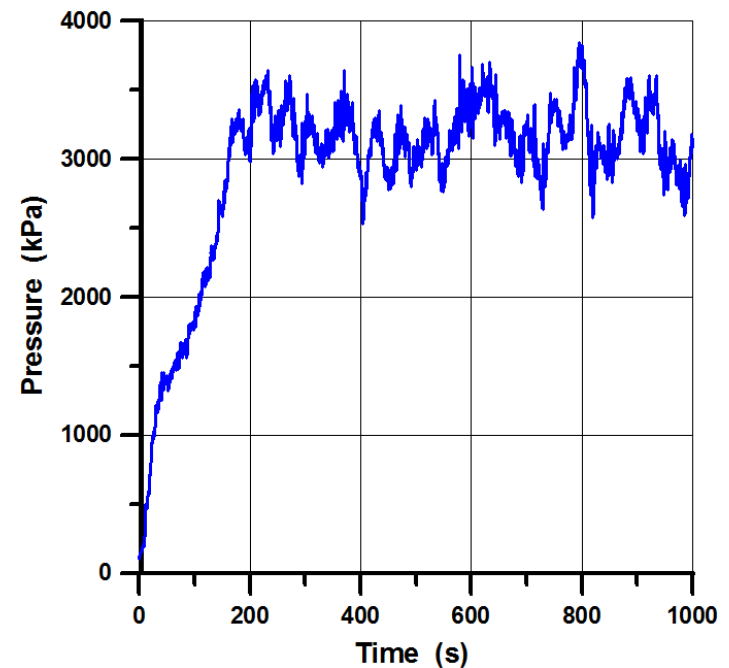
Snap-shot of riser shape after static analysis



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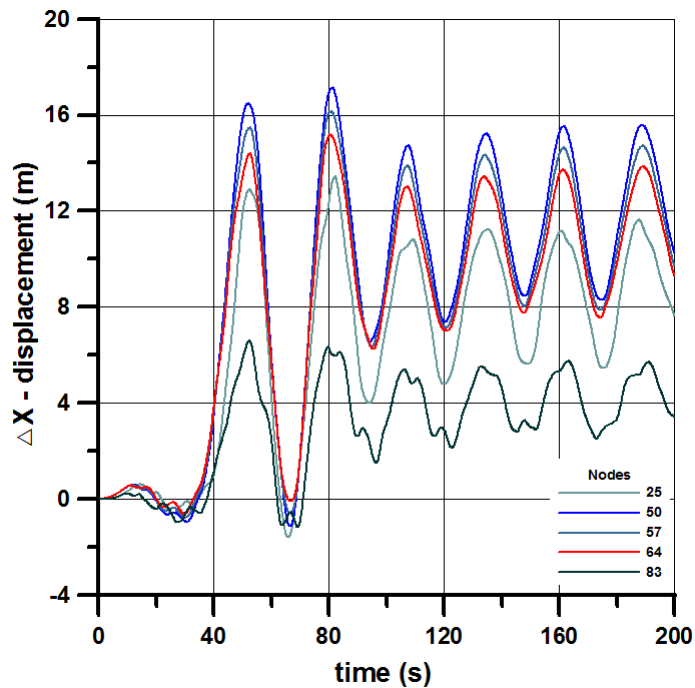
Snap-shots of riser shapes during time integration



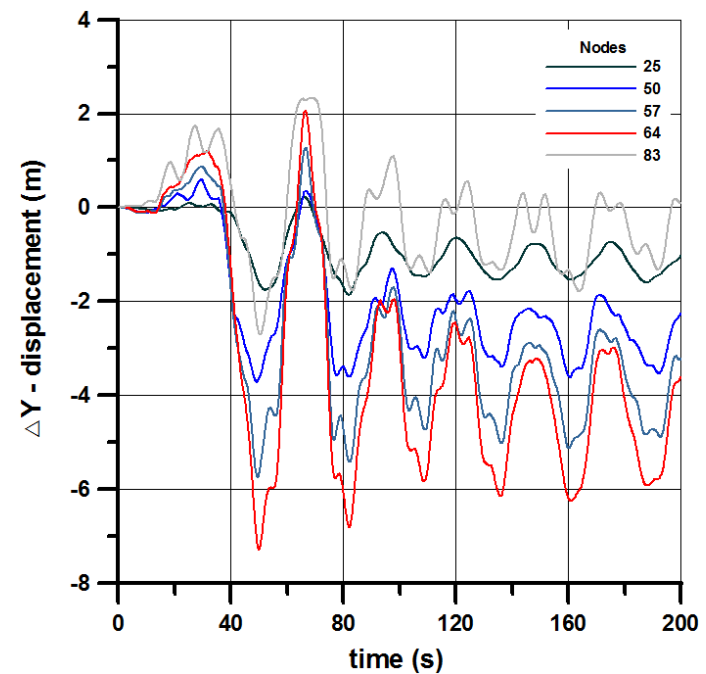
Time history of slug flow inlet pressure

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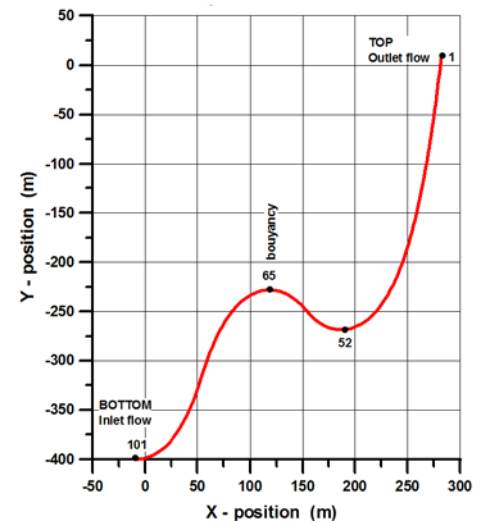
Time history of displacements



Time history of ΔX displacements

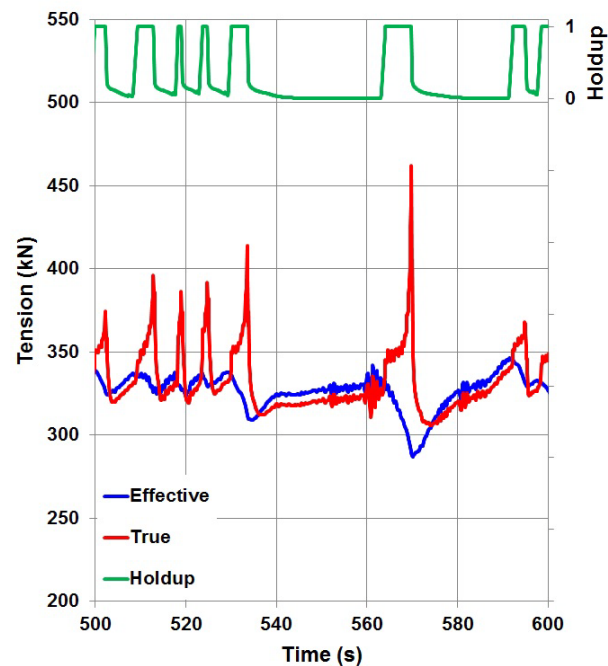


Time history of ΔY displacements

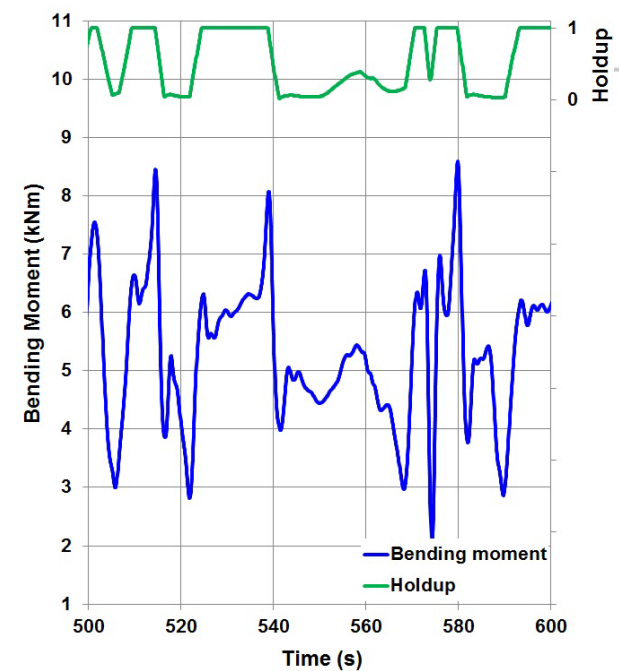


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Time Series



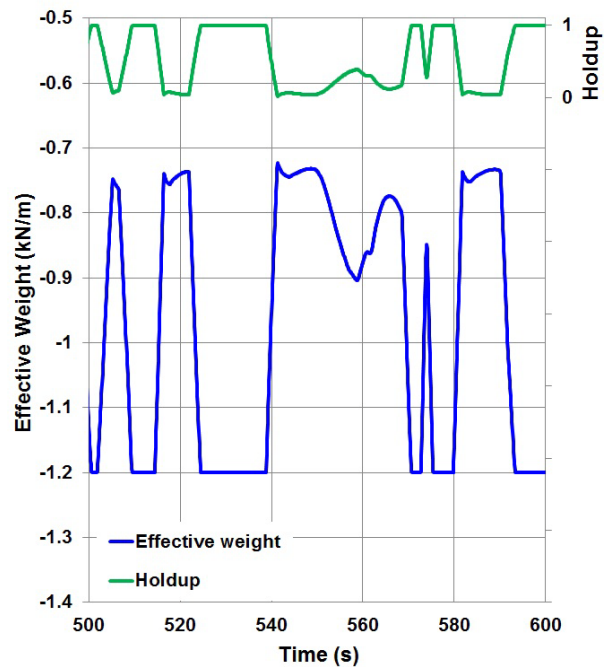
Time history of top tension



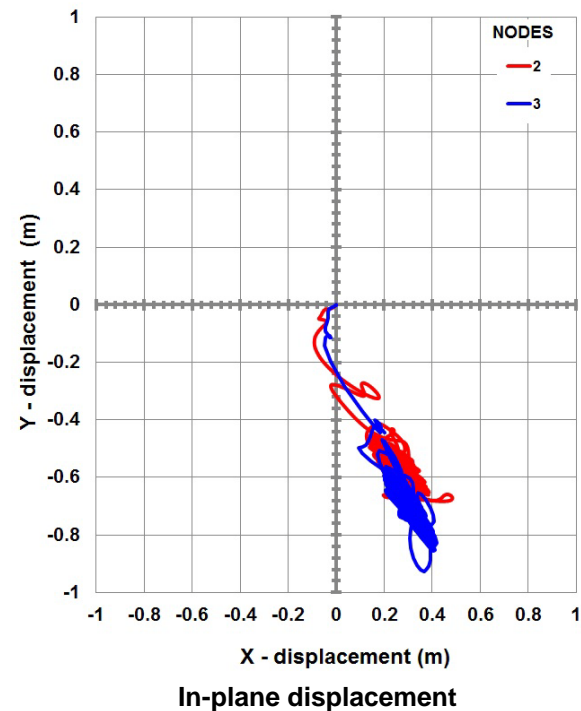
Time history of bending moment at node 29

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Time Series



Time history of effective weight at node 29



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Final Remarks:

- A computational tool for analyzing of the interaction fluid-structure has been built.
- *In-house* codes worked as independent, interconnected by information feedback.
- Lazy-wave riser configurations.
- Undergoing a hydrodynamic and severe slugging.
- Riser response influenced in the behavior of slug flow.
- Slug flow generated displacements, moments and tensions variations.

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Thank you very much !!!