



Inverse Analysis of VIV Experiments

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Outline

- Background
- Objective
- Methodology
- Application
- Conclusions

VIV and Offshore Structures

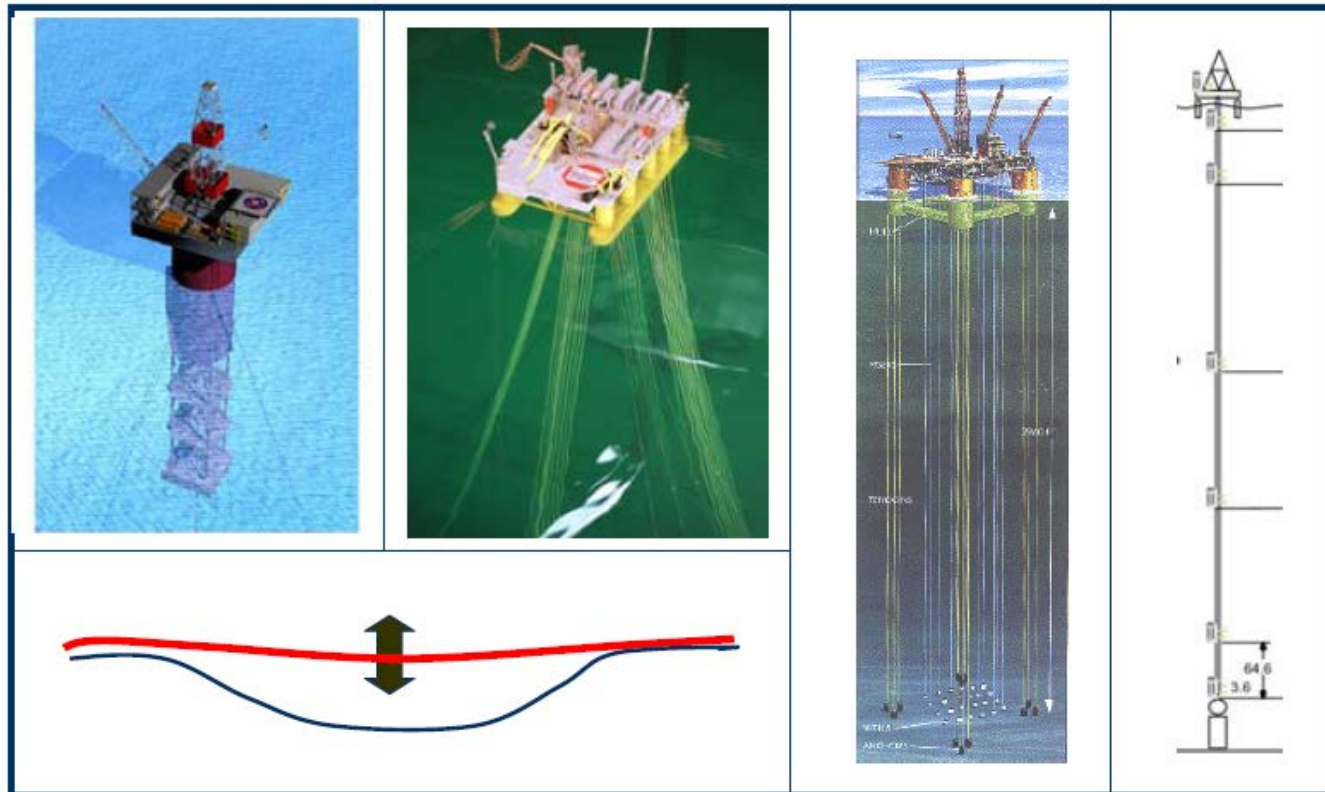


Figure from Baarholm

- ☐ Fatigue damage
- ☐ Amplified drag force

Empirical VIV Prediction Models

- Industrial tools:

- VIVANA, Larsen
- SHEAR7, Vandiver
- VIVA, Triantafyllou

- Hydrodynamic Force Model

- Empirical hydrodynamic force coefficient database
- Rigid cylinder VIV test

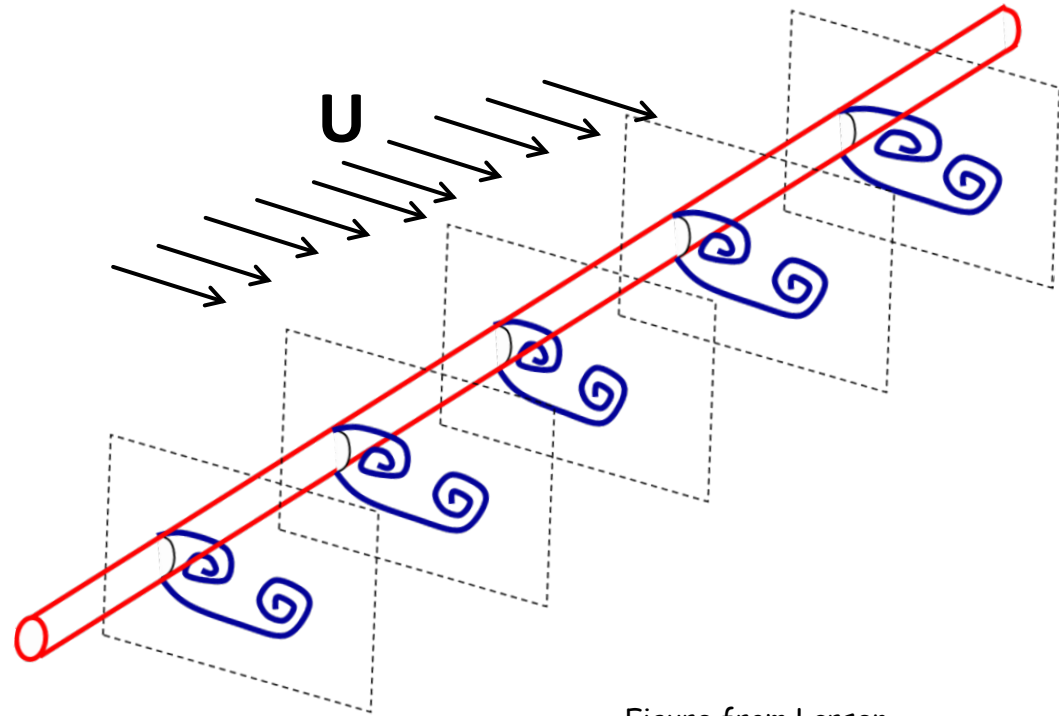


Figure from Larsen

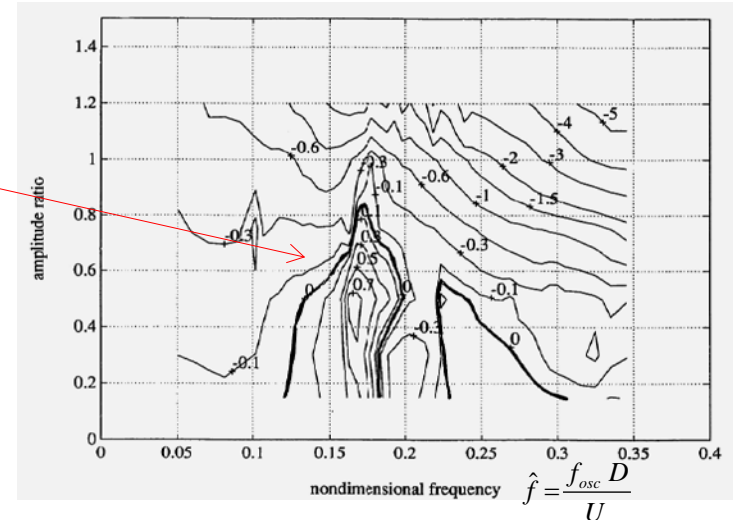
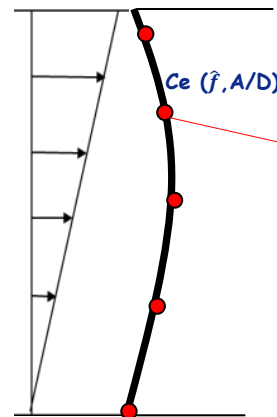
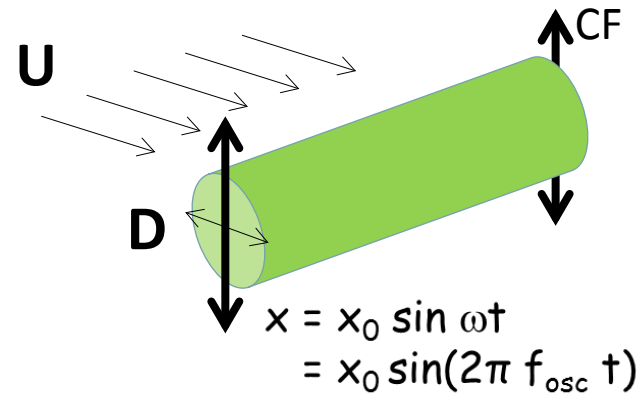
Hydrodynamic Force Coefficient Database

2D Rigid Cylinder VIV Test

- Forced Harmonic Motions
- Forces are directly measured
- Excitation coefficient, C_e
- Added mass coefficient, C_a

Force coefficient database

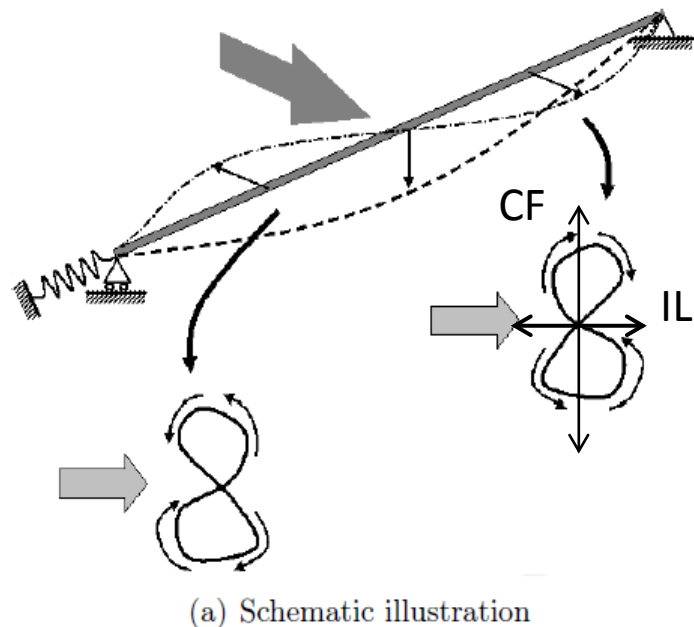
- $C_e(\hat{f}, A/D)$
- $C_a(\hat{f}, A/D)$



Gopalkrishnan, 1993



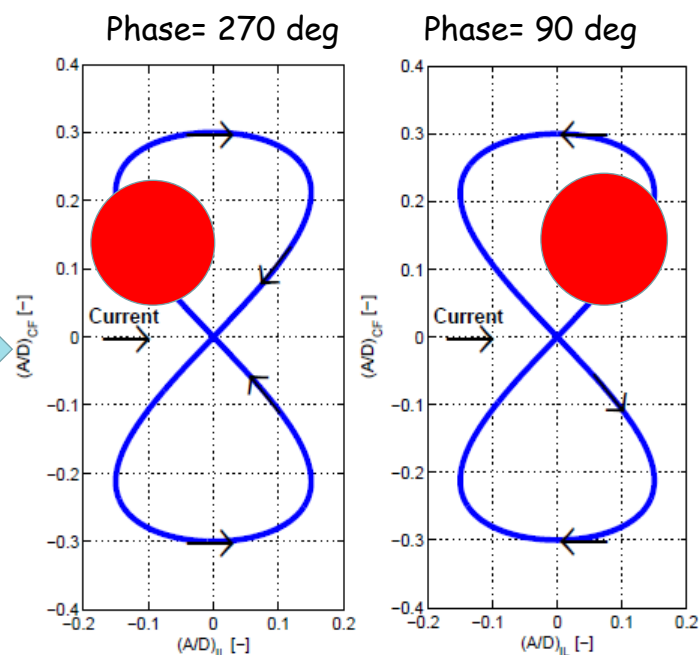
IL and CF Interaction



There is still lack of a complete load interaction model

Current

Rigid cylinder forced motion test



(b) Tested orbitals

Aronsen, et al (2007)

3D VIV Experiments with Flexible Cylinders

❑ Experiments (1997 - 2012)

Rotating Rig Tests

Hanøytangen Test

Ormen Lange Test

NDP High Mode VIV Test

MIAMI Tests

Shell VIV Tests

Other tests...

❑ Uniform or sheared flow

❑ With/without suppression devices

❑ Response frequency, amplitudes, and modal information are often analyzed

No direct force measurements along the flexible cylinder

Acceleration or/and bending strain measurements

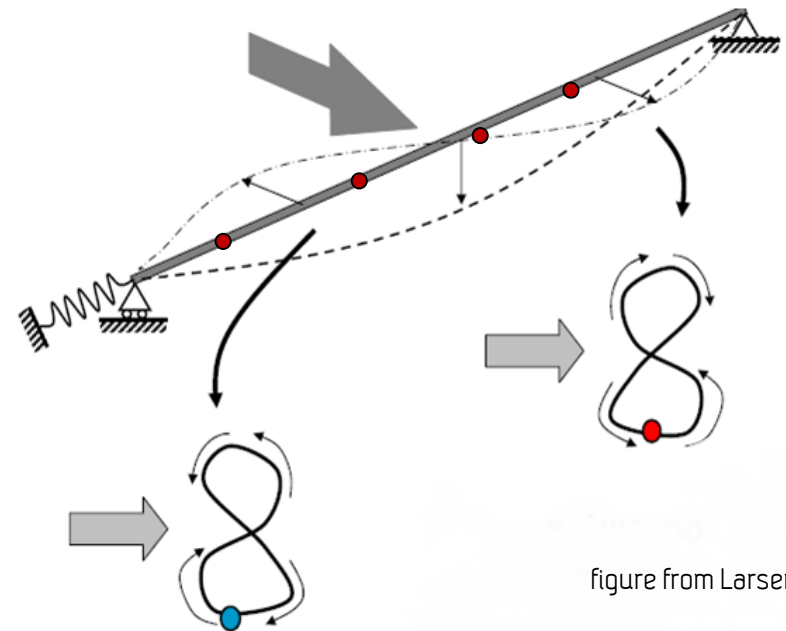
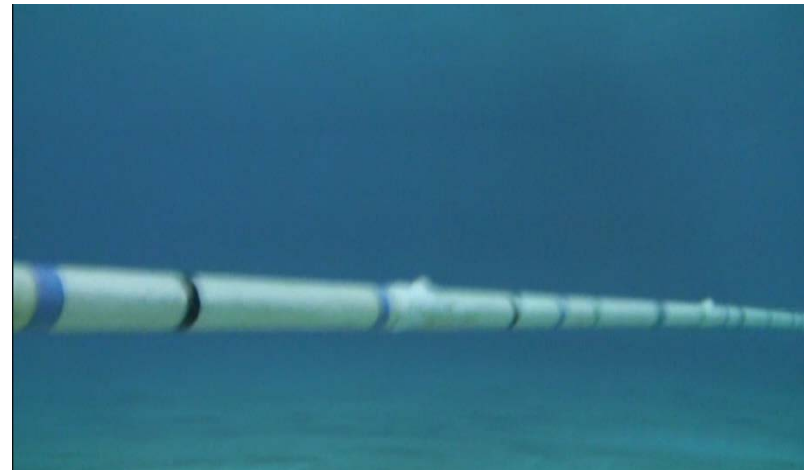
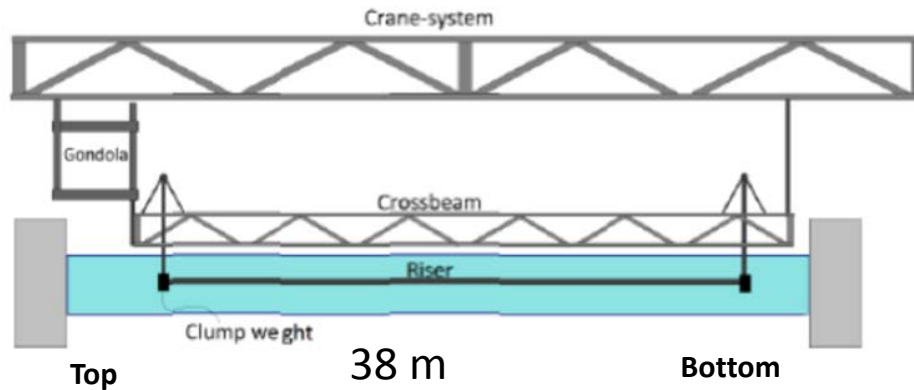


figure from Larsen

3D VIV Experiments with Flexible Beams



No direct force measurements along the flexible cylinder

Research Objectives

- Obtain a tool to identify hydrodynamic forces/coefficients from VIV experiments with flexible cylinders
- Improve the existing force model/force coefficient database in empirical programs
- Understand better VIV loading mechanism of flexible cylinders – IL and CF interaction



Hydrodynamic Force Identification by Inverse Analysis

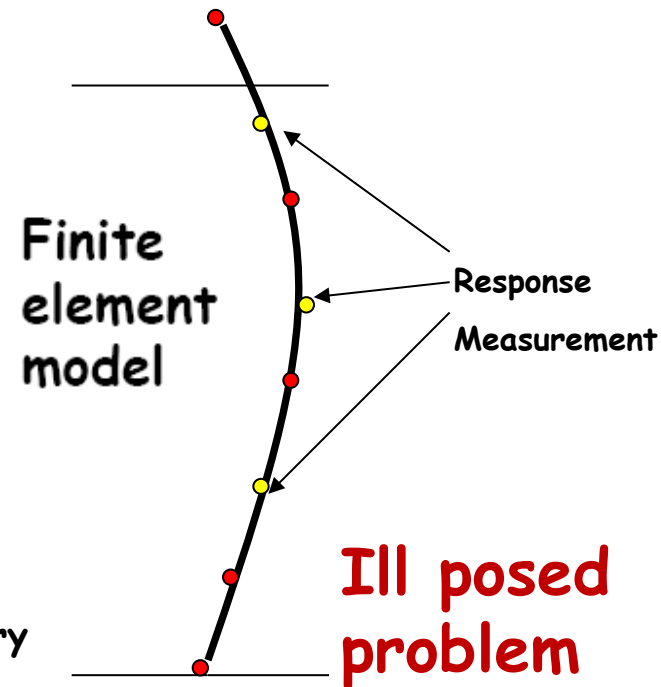
The Dynamic Equilibrium Equation

$$\begin{array}{cccc} \text{Structural} & \text{Structural} & \text{Structural} & \text{Hydrodynamic} \\ \text{Mass} & \text{Damping} & \text{Stiffness} & \text{forces} \\ \text{M} \ddot{\mathbf{r}} + \mathbf{C} \dot{\mathbf{r}} + \mathbf{K} \mathbf{r} = \mathbf{R} \end{array}$$

Identify hydrodynamic forces along the pipe

Method 1: Direct Inverse Analysis

Method 2: Inverse Analysis based on Optimal Control Theory



Method 1: Direct Inverse Analysis

Response Reconstruction from Measurements by Modal Approach

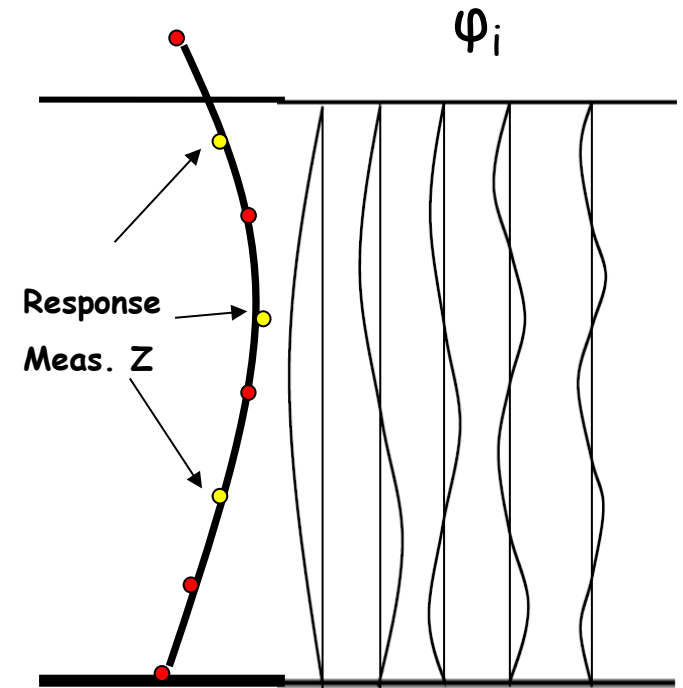
$$Z(t) = \sum_{n=1}^{\infty} w_n(t) \varphi_n \quad \text{or} \quad \mathbf{Z} = \mathbf{\Phi}^T \mathbf{w}$$

$$\mathbf{w} = (\mathbf{\Phi}^T \mathbf{\Phi})^{-1} \mathbf{\Phi}^T \mathbf{Z}(t)$$

$$\mathbf{r} = \overline{\mathbf{\Phi}} \mathbf{w}$$

Estimate Forces along the Pipe

$$\mathbf{M}\ddot{\mathbf{r}} + \mathbf{C}\dot{\mathbf{r}} + \mathbf{K}\mathbf{r} = \mathbf{R}$$





Method 2: Inverse Analysis Based on Optimal Control Theory

State Space Form of Dynamic Equilibrium Equation

$$\dot{\mathbf{X}}(\mathbf{t}) = \mathbf{A}\ddot{\mathbf{X}}(\mathbf{t}) + \mathbf{B}\mathbf{F}(\mathbf{t})$$

$$\mathbf{Z}(\mathbf{t}) = \mathbf{G}\mathbf{X}(\mathbf{t})$$

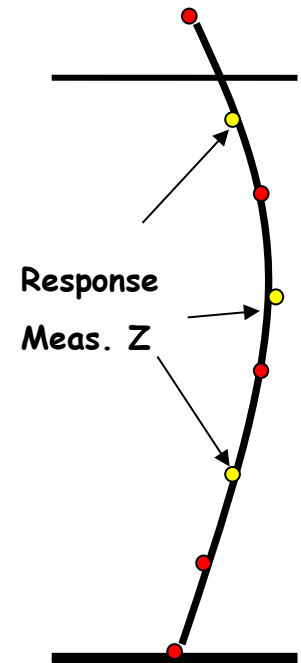
Cost Functions

$$\mathbf{j}_Z(\mathbf{t}) = \frac{1}{2}(\mathbf{Z}_0 - \mathbf{Z})^T \mathbf{Q}_{ZZ}(\mathbf{Z}_0 - \mathbf{Z}), \quad \text{where} \quad \mathbf{Q}_{ZZ} = \frac{1}{\sigma_z^2} \mathbf{I}$$

$$\mathbf{j}_F(\mathbf{t}) = \frac{1}{2}\mathbf{F}^T \mathbf{Q}_{FF} \mathbf{F}, \quad \text{where} \quad \mathbf{Q}_{FF} = \frac{1}{\sigma_F^2} \mathbf{I}$$

Solving Constrained Optimization

$$\mathbf{J} = \int \left(\frac{1}{2} \mathbf{X}^T \mathbf{Q}_{XX} \mathbf{X} + \mathbf{Q}_X \mathbf{X} + \frac{1}{2} \mathbf{F}^T \mathbf{Q}_{FF} \mathbf{F} \right) dt, \quad \min_{\mathbf{X}, \mathbf{F}} \mathbf{J} \text{ subjected to } \dot{\mathbf{X}}(\mathbf{t}) = \mathbf{A}\ddot{\mathbf{X}}(\mathbf{t}) + \mathbf{B}\mathbf{F}(\mathbf{t})$$

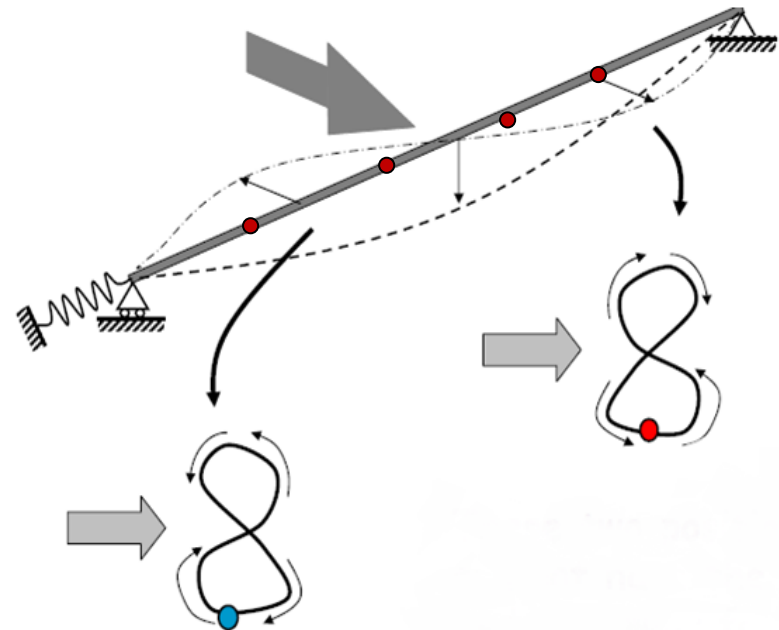


Application of Inverse Analysis on VIV Experiments with Flexible Cylinders

Identify hydrodynamic forces/coefficients from VIV experiments with flexible cylinders

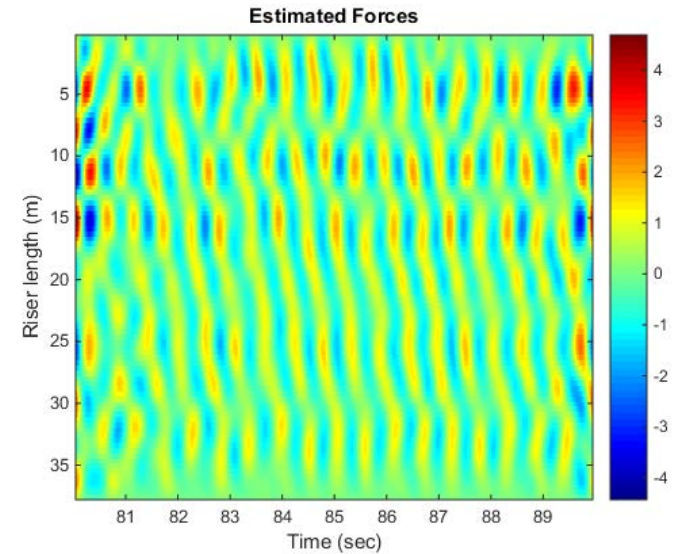
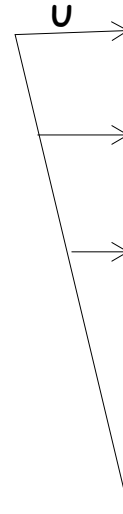
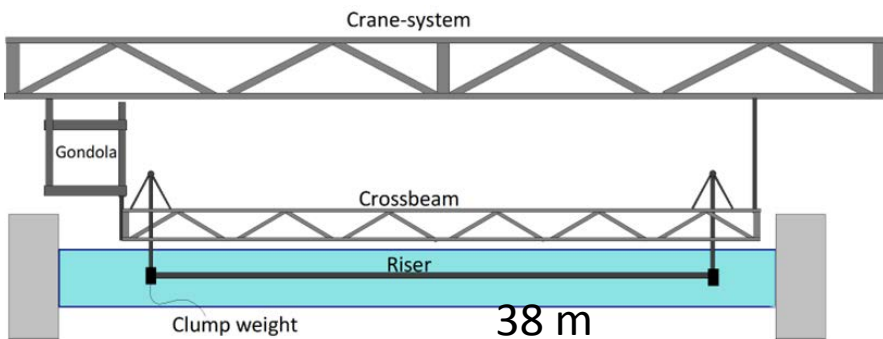
- Rotating Rig Test, 1996, 2003
- Hanøytangen Test, 1997
- NDP High Mode VIV Test, 2003
- Shell VIV Test, 2011

Acceleration or/and bending strain measurements



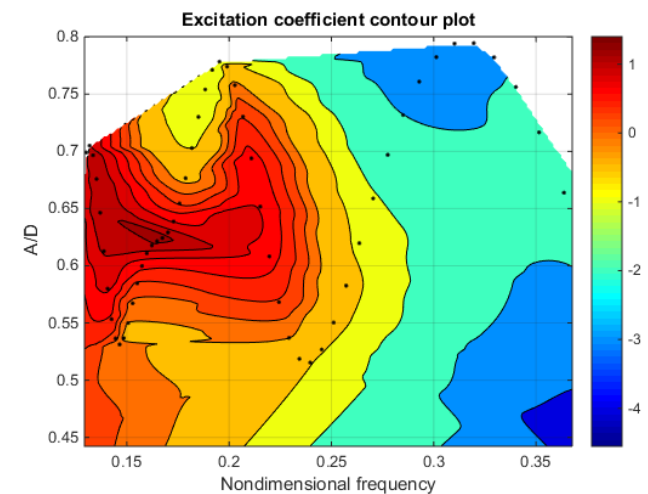
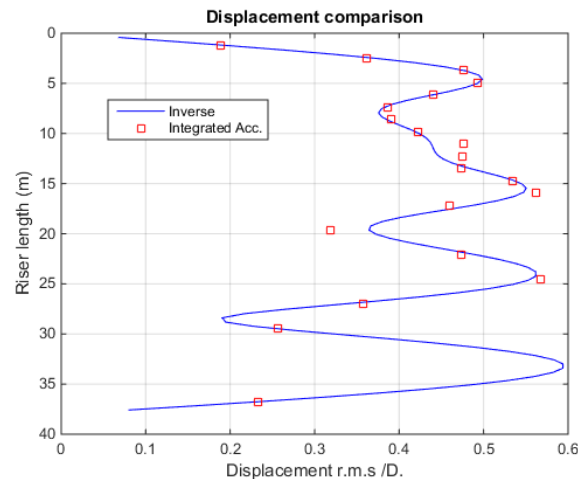
Application - Force Identification

Shell VIV Test, 2011



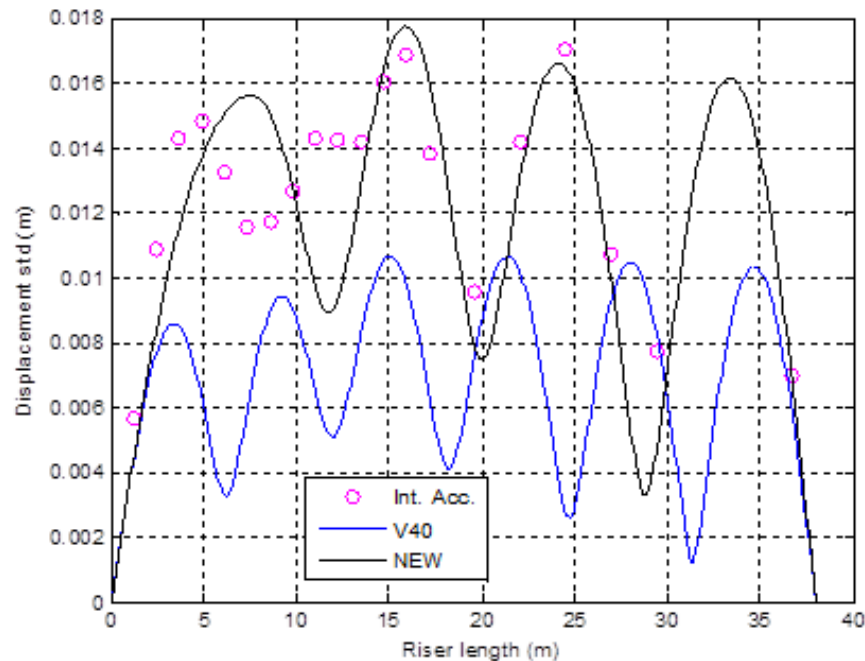
- CF response measurements:

22 accelerometers
30 strain measurements

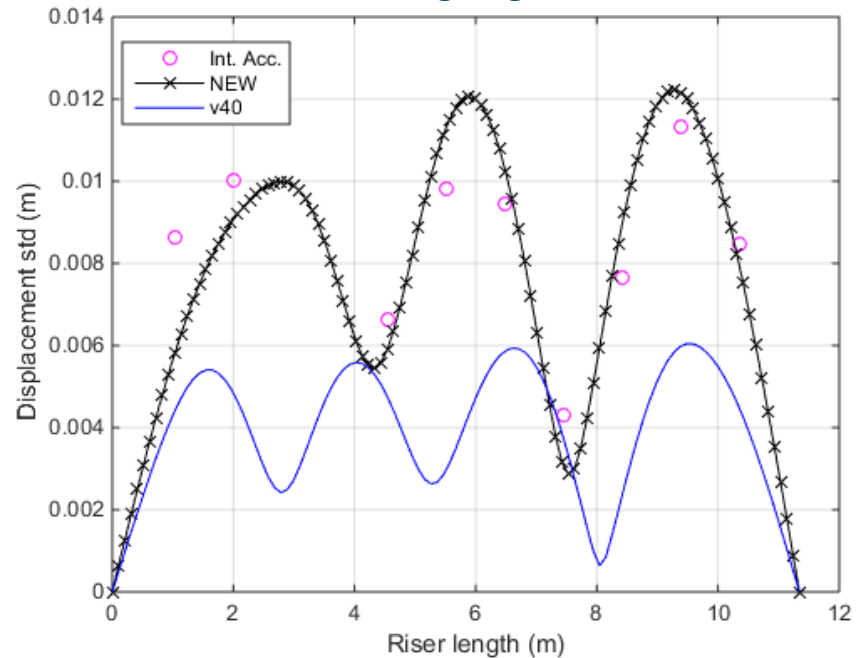


Application – VIVANA Prediction

Shell VIV Test



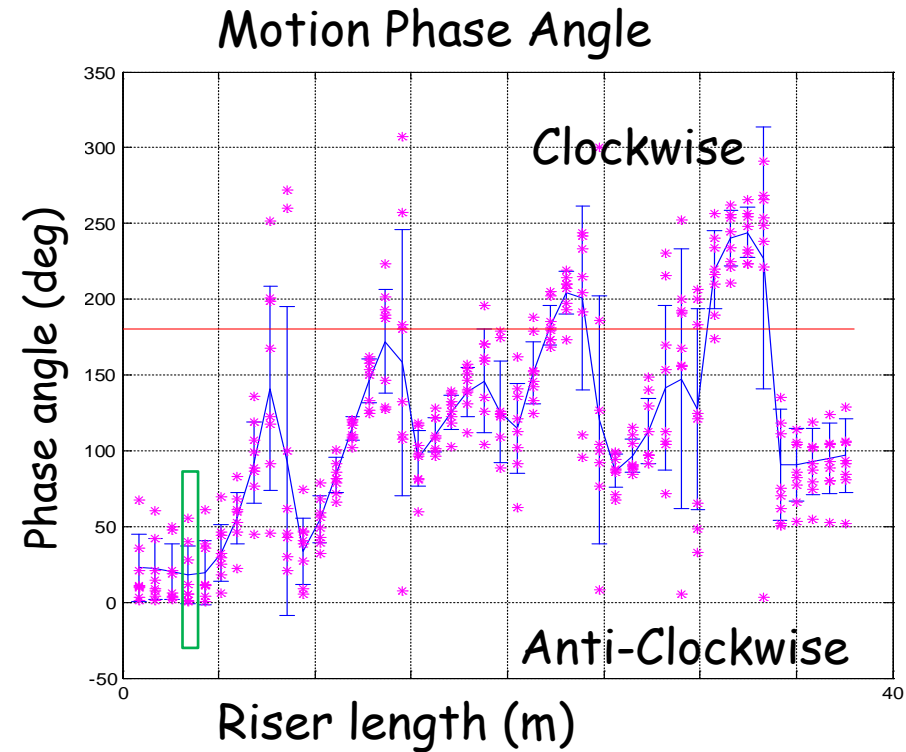
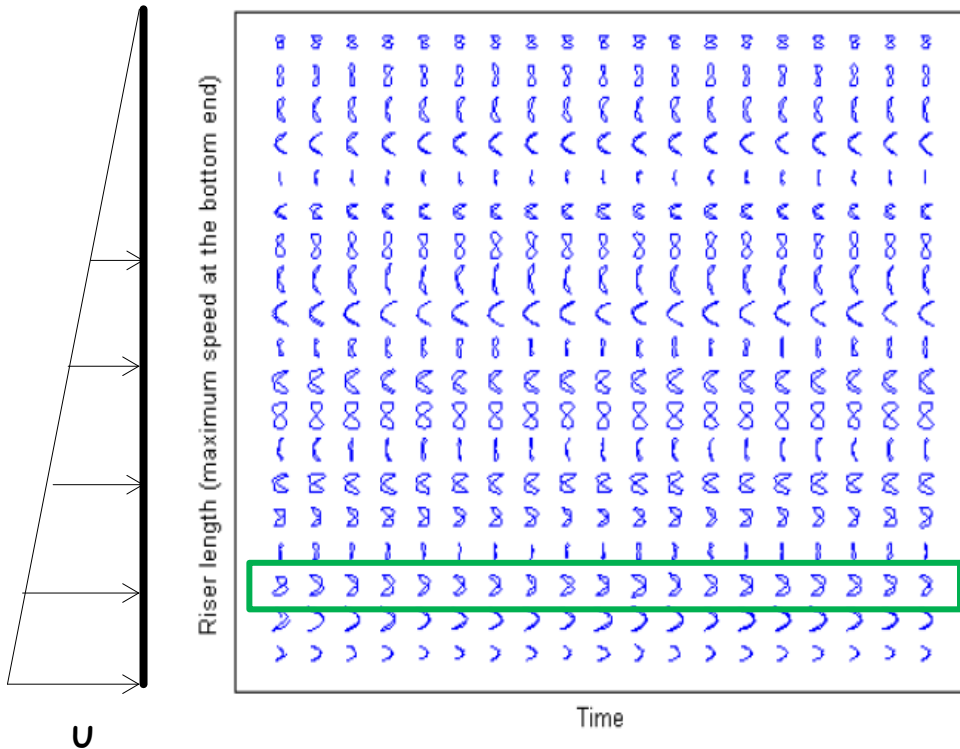
Rotating Rig Test



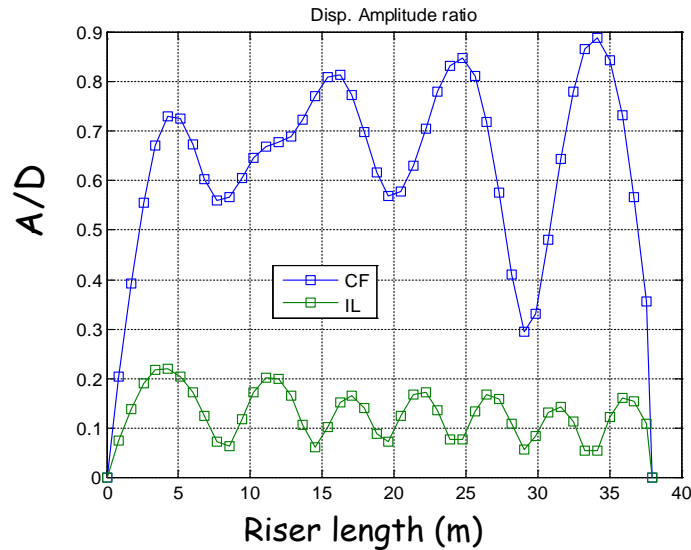
☐ Correct response frequency

☐ Improvement in response prediction

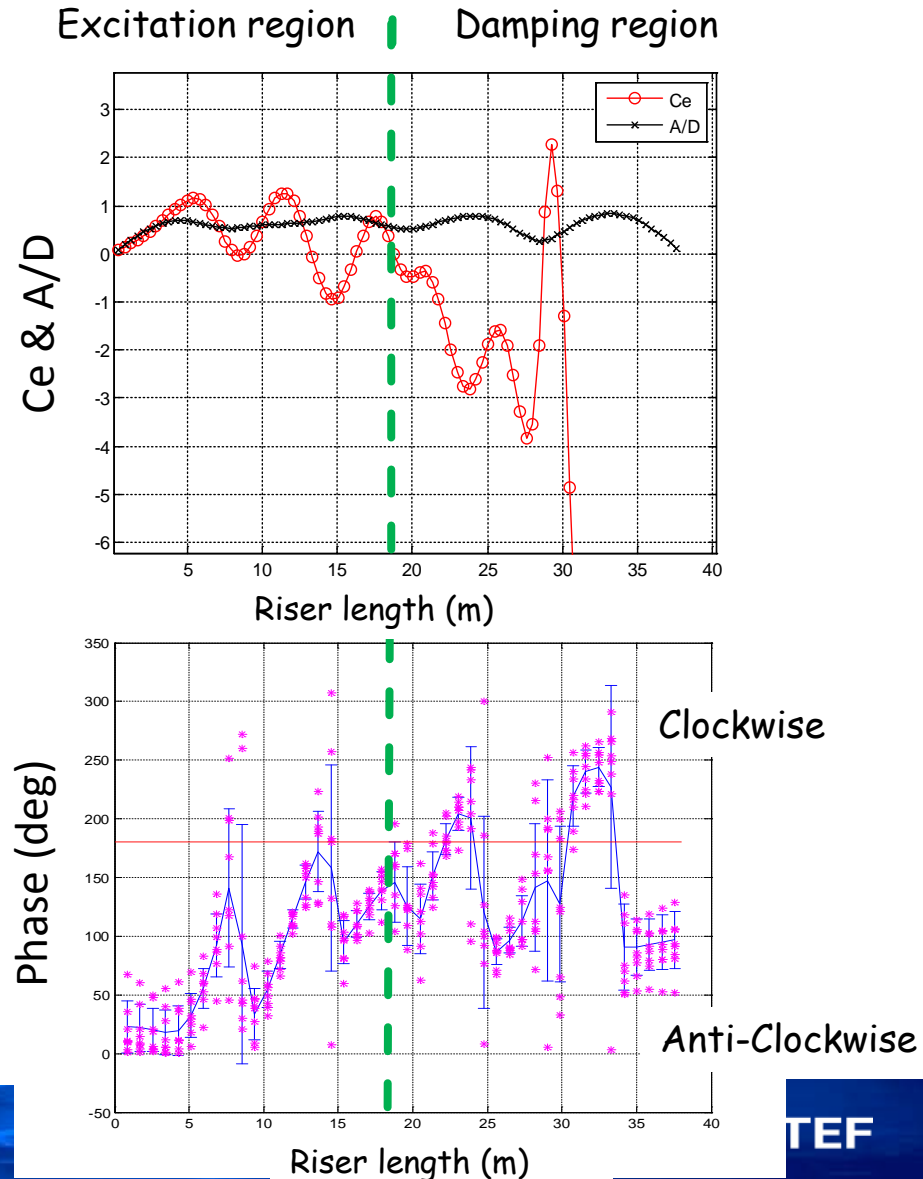
Application - IL and CF Interaction



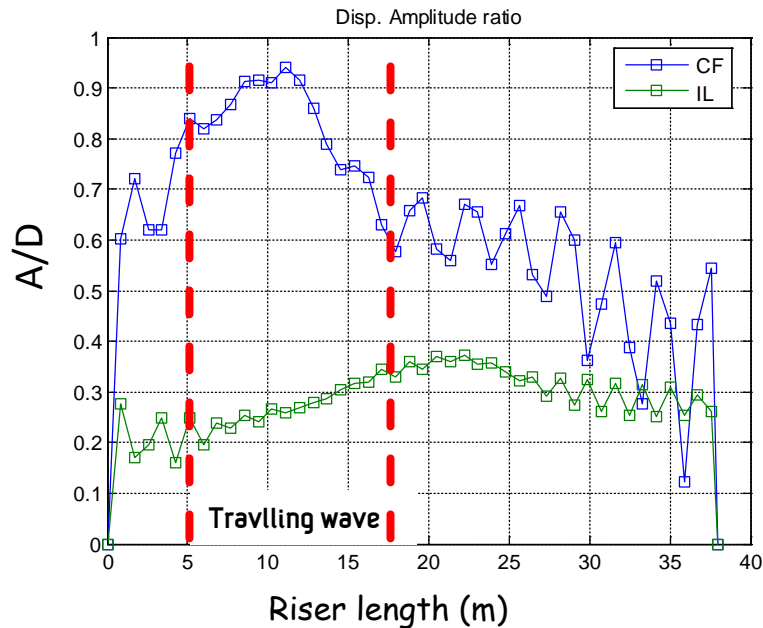
Application - IL and CF Interaction



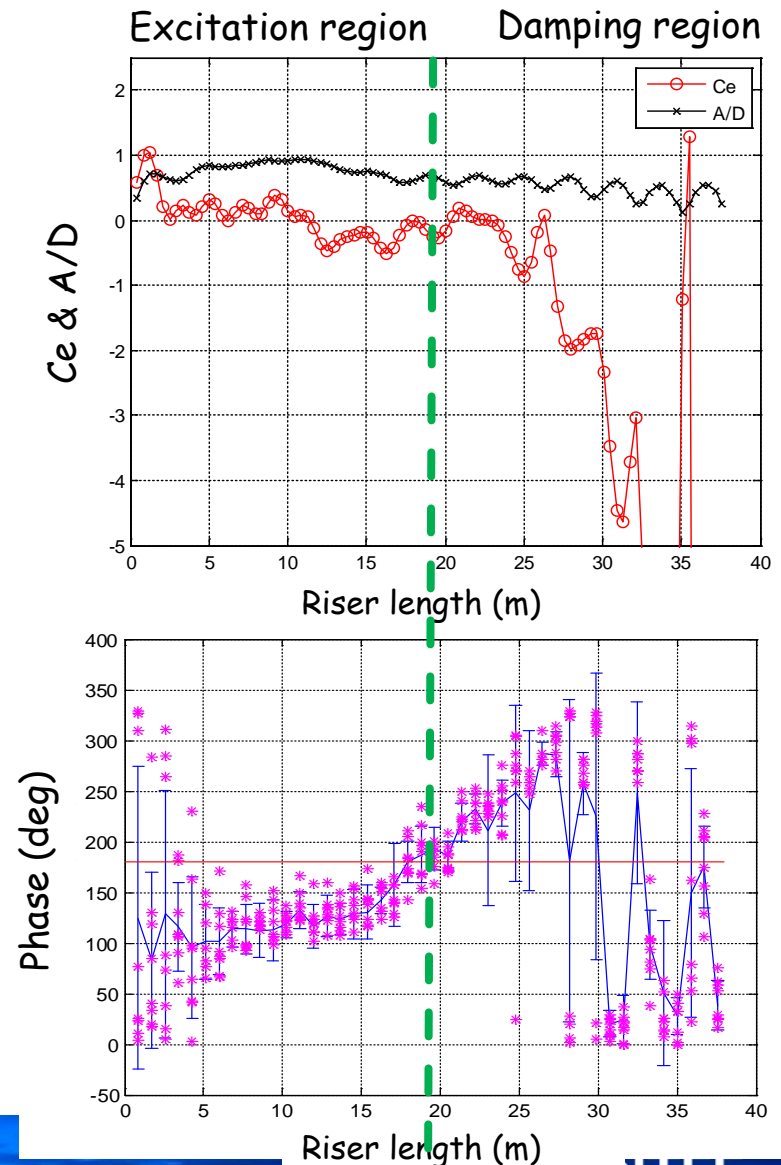
- Zigzag phase variation + drift
- Positive C_e for phase < 180 deg (excitation region)
- Consistent with DNS simulation (Bourguet et al, 2011)
- Wu et al, OMAE2014-24559



Application - IL and CF Interaction



- No zigzag variation due to stronger travelling waves
- Positive C_e for phase < 180 deg (excitation region)



Conclusions

- Inverse analysis method is a valuable tool to obtain hydrodynamic forces/coefficients from VIV experiments with flexible cylinders
- The identified hydrodynamic forces/coefficients can be used to improve existing load models
- Phase between IL and CF displacements is a key parameter to understand the interaction and it is strongly coupled with force coefficients

Thank You!

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SINTEF

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