

Time domain analysis of vortex-induced vibrations (VIV)

Introduction

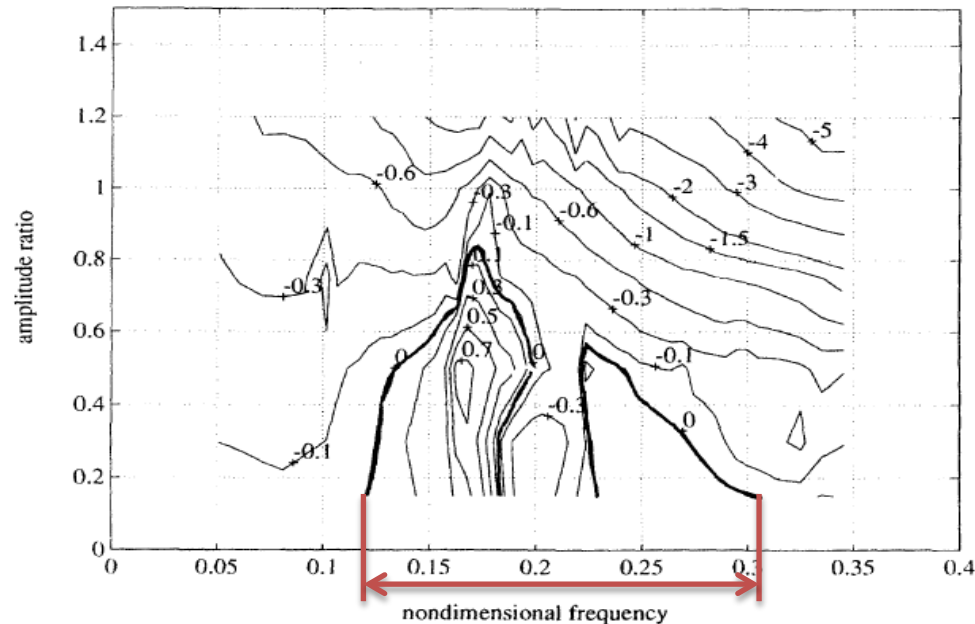
- About me:
 - Mats Jørgen Thorsen
 - PhD 2012-2016
 - Topic: VIV
 - Supervisors:
 - Svein Sævik
 - Carl M. Larsen

Motivation

- Traditional VIV analysis tools operate in frequency domain.
- Freq. domain limitations:
 - Linear structure
 - Stationary conditions (e.g. constant current velocity)
- A time domain formulation would allow for:
 - Nonlinear effects (tension variations, soil contact, etc.)
 - Time varying currents
 - Interaction with other loads (e.g. internal flow)

VIV fundamentals

- For a fixed cylinder, $f_s = St \frac{U}{D}$, where $St \approx 0.2$
- Forced vibration experiment, Gopalkrishnan (1993):



- For a vibrating cylinder, the vortex shedding synchronizes with the cylinder motion over a range of frequencies

Synchronization

- Inspiration:
 - Fireflies!



- Gather in very large groups and flash in unison
- Researchers have studied/modeled their synchronization

Fireflies



- Hanson (1978) did experiments with periodically flashing light. How does the firefly synchronize?
 - ω_0 : Firefly natural frequency
 - ω_e : Frequency of flashing light
- Findings:
 - For a range of ω_e *close to* ω_0 the firefly synchronizes
 - If ω_e is too far from ω_0 , the firefly does not keep up.
- Note similarities with vortex shedding!

Firefly modeling

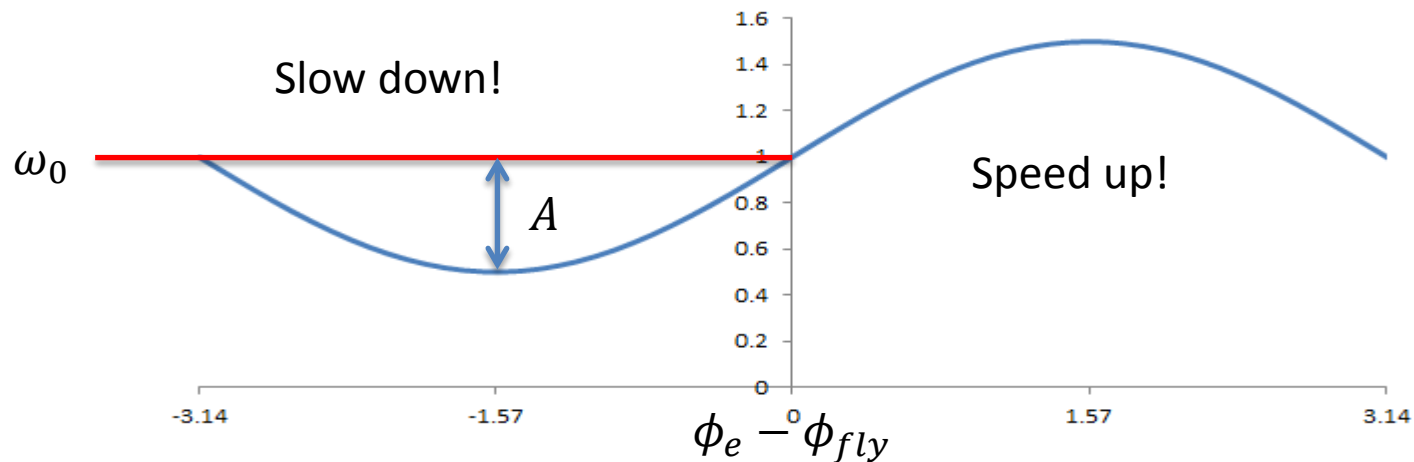
ϕ_e : Phase of flashing light. Flash when $\phi_e = 0$

$\frac{d\phi_e}{dt} = \omega_e$: Frequency of flashing light

ϕ_{fly} : Phase of firefly

- Model proposed by Ermentrout and Rinzel (1984):

$$\frac{d\phi_{fly}}{dt} = \omega_0 + A \sin(\phi_e - \phi_{fly})$$



Back to VIV

- Assume the cross-flow excitation force can be expressed as $\frac{1}{2}\rho D U^2 C_v \cos \phi_{exc}$
 - ϕ_{exc} : Phase of the cross-flow excitation force
 - $\phi_{\dot{y}}$: Phase of cylinder cross-flow velocity

- Synchronization model:

$$\frac{d\phi_{exc}}{dt} = H(\underbrace{\phi_{\dot{y}} - \phi_{exc}}_{\text{Phase difference between velocity and force}})$$

(Similar to Ermentrout and Rinzel)

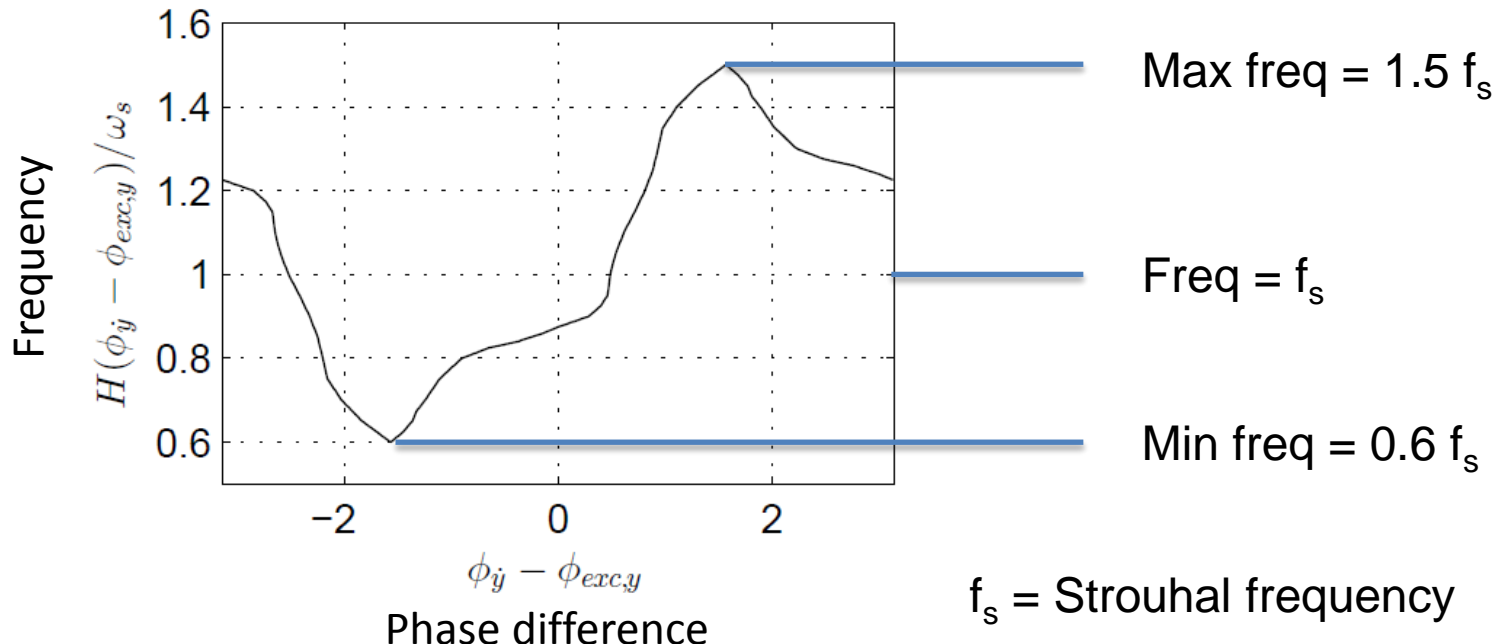
- How to find H ?

Finding H , the synchronization function

- In the range of synchronization, assume

$$C_{exc}(\omega) = C_{exc,max} \cos(\theta(\omega))$$

- Plot ω versus θ based on VIVANA's C_{exc} :



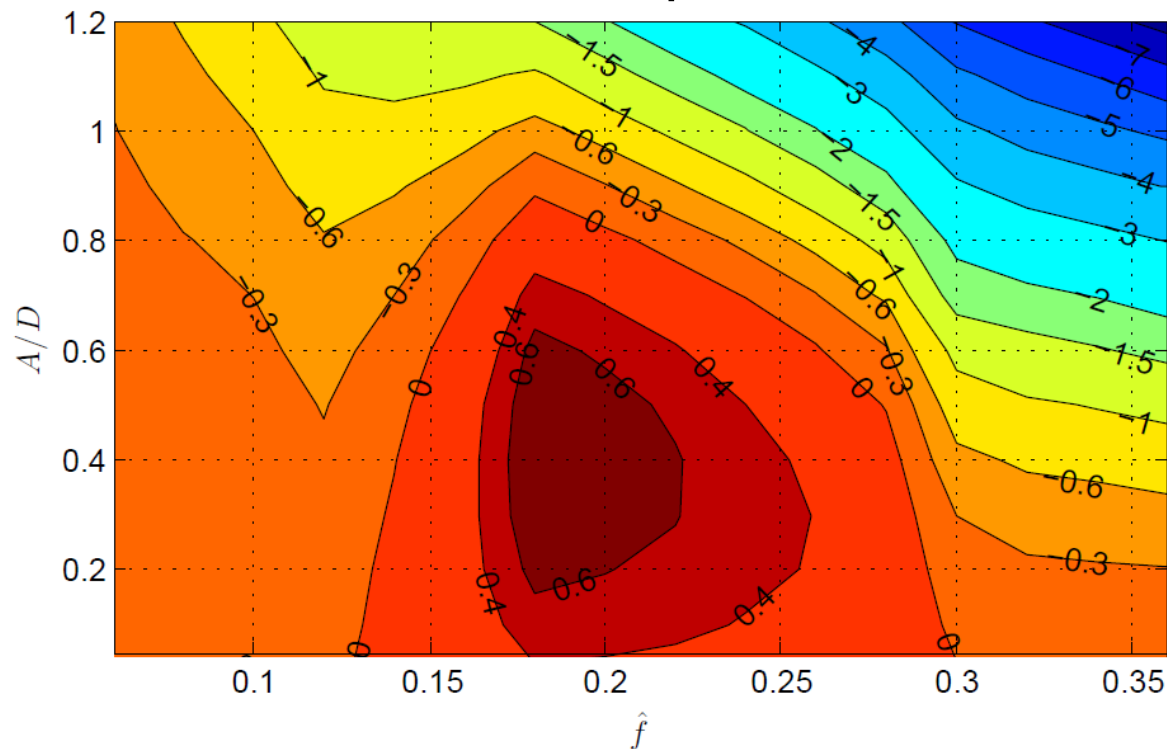
Cross-flow hydrodynamic force model

$$F_{fluid,y} = \underbrace{\frac{1}{2}\rho DC_v U^2 \cos \phi_{exc,y}}_{\text{excitation}} - \underbrace{\frac{1}{2}\rho DC_{y1} U \dot{y} - \frac{1}{2}\rho A_y C_{y2} |\dot{y}| \dot{y}}_{\text{damping}} - \underbrace{\frac{\rho \pi D^2}{4} C_{ay} \ddot{y}}_{\text{added mass}}$$

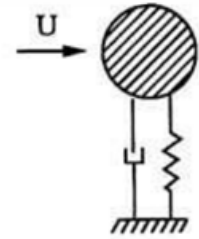
1. Excitation with synchronization
2. Hydrodynamic damping
3. Added mass, $C_{ay} = 1$

Results

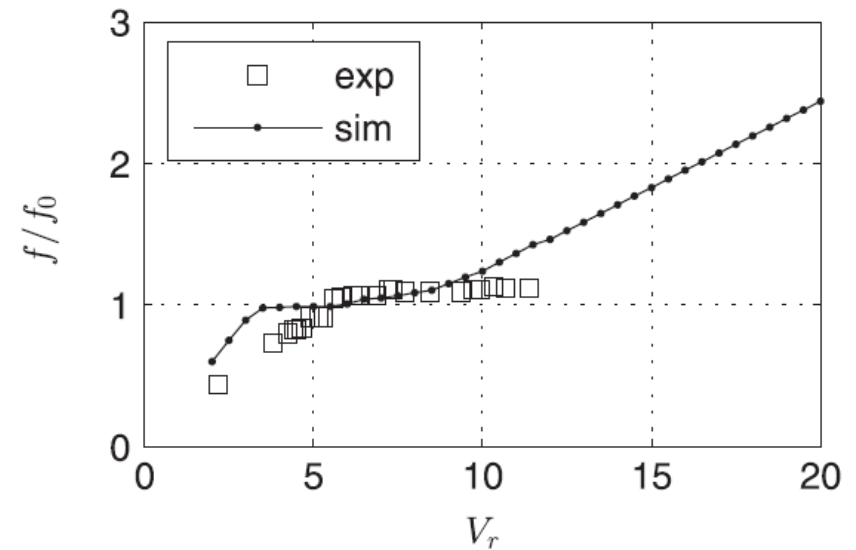
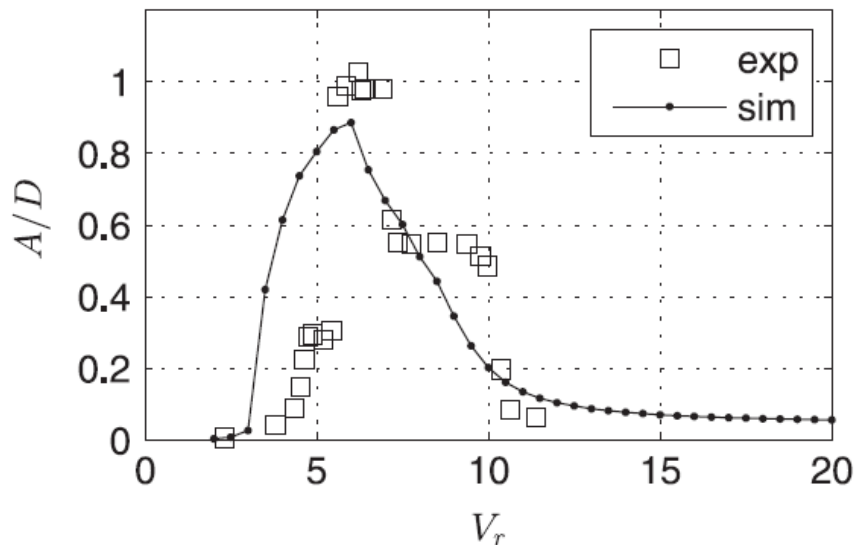
- Does the model provide a realistic description of the energy transfer between fluid and structure?
- Simulated forced vibration experiment:



Results



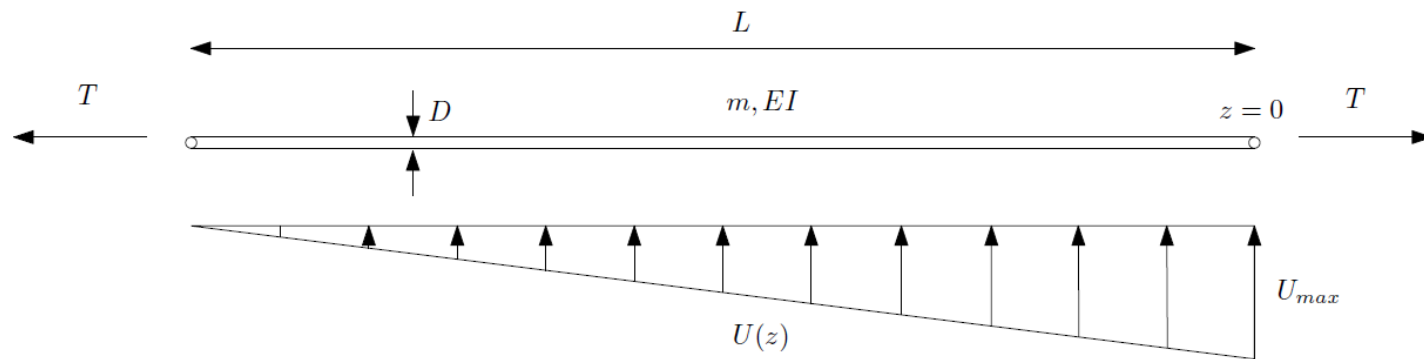
- Can the model predict the amplitudes and frequencies seen in classical 1-DOF experiments?



Simulation compared to experiment (Govardhan & Williamson, 2000)

Results

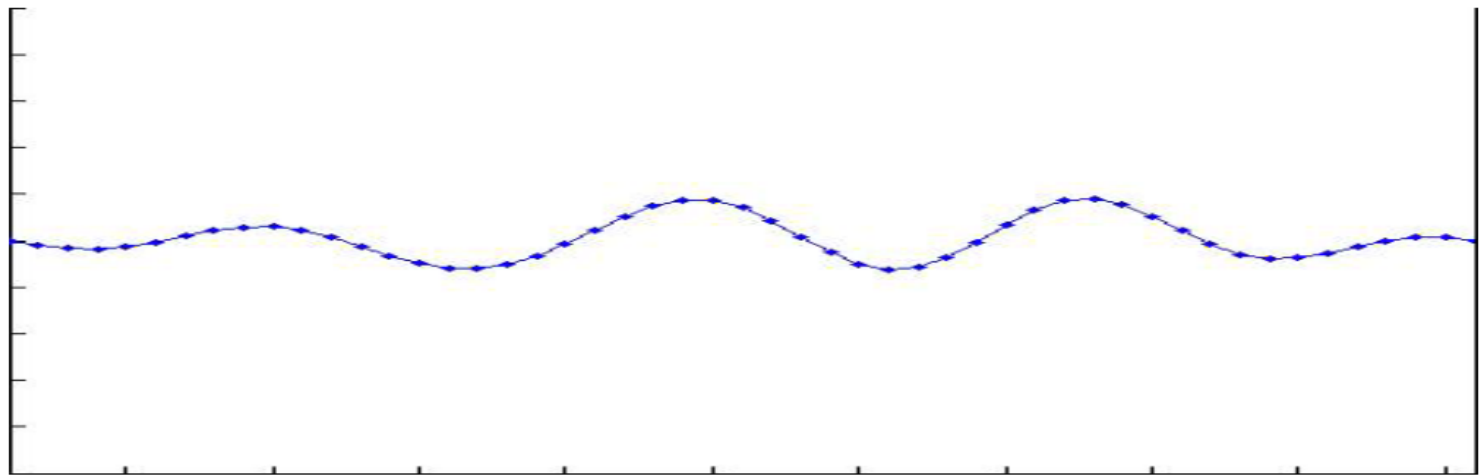
Elastic cylinder in shear flow (NDP High Mode VIV tests)



- Linear beam FE model
- Hydrodynamic force calculated at every node
- Time integration using Newmark- β

Results

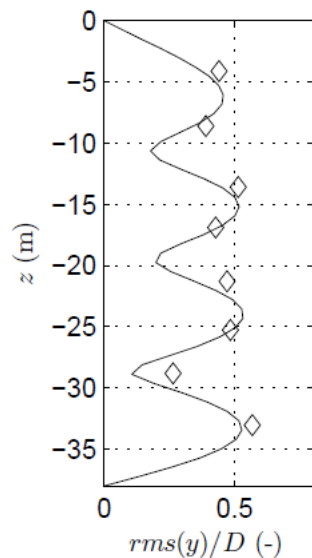
Elastic cylinder in shear flow



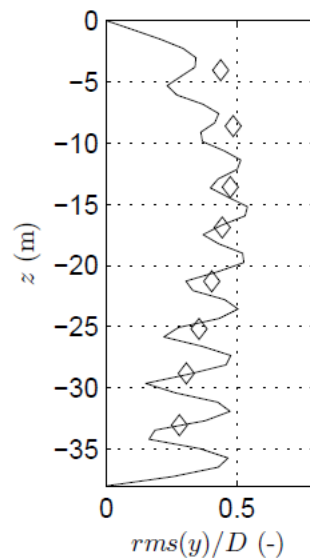
Results

Elastic cylinder in shear flow

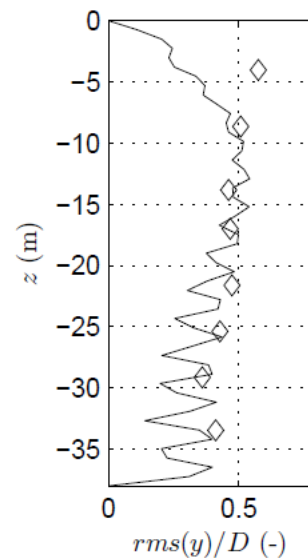
Cross-flow response compared to experiment:



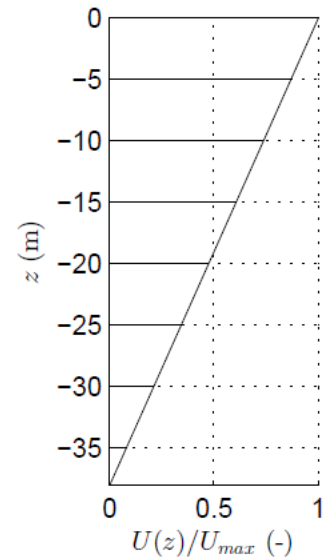
(a) $U_{max} = 0.6 \text{ m/s}$



(b) $U_{max} = 1.3 \text{ m/s}$



(c) $U_{max} = 2.0 \text{ m/s}$

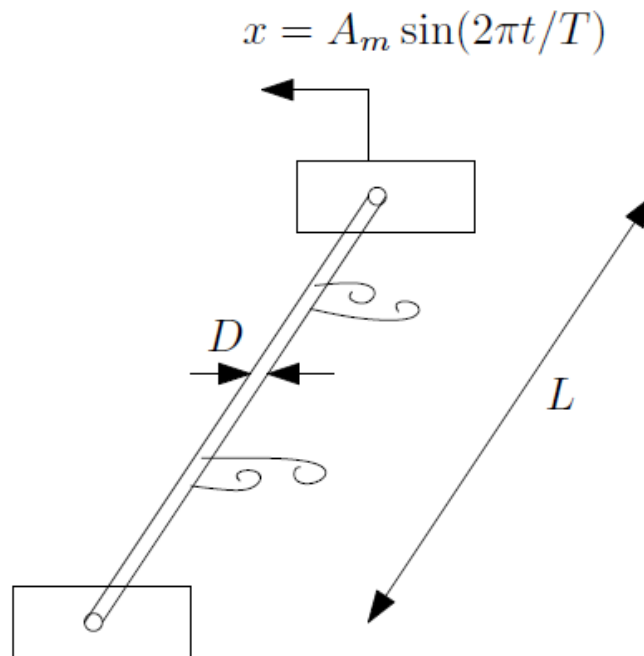


(d) Current profile

solid lines = simulated
diamonds = measured

Results

- Flexible cylinder in oscillating flow
- Experiments by Fu et al. (2014)

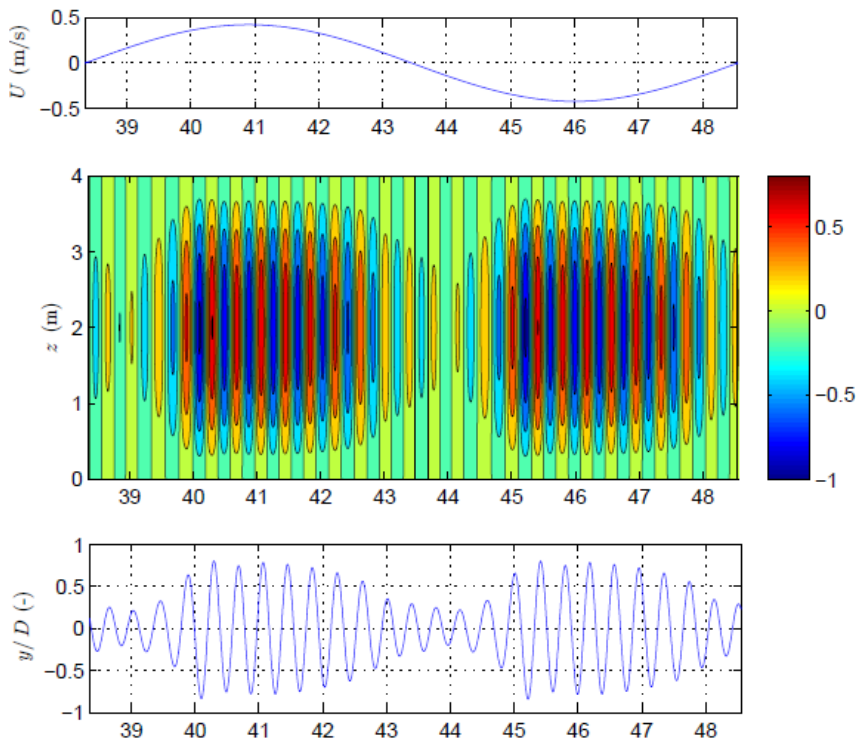


$$KC = \frac{U_{\max} T}{D} = \frac{2\pi A_m}{D}$$

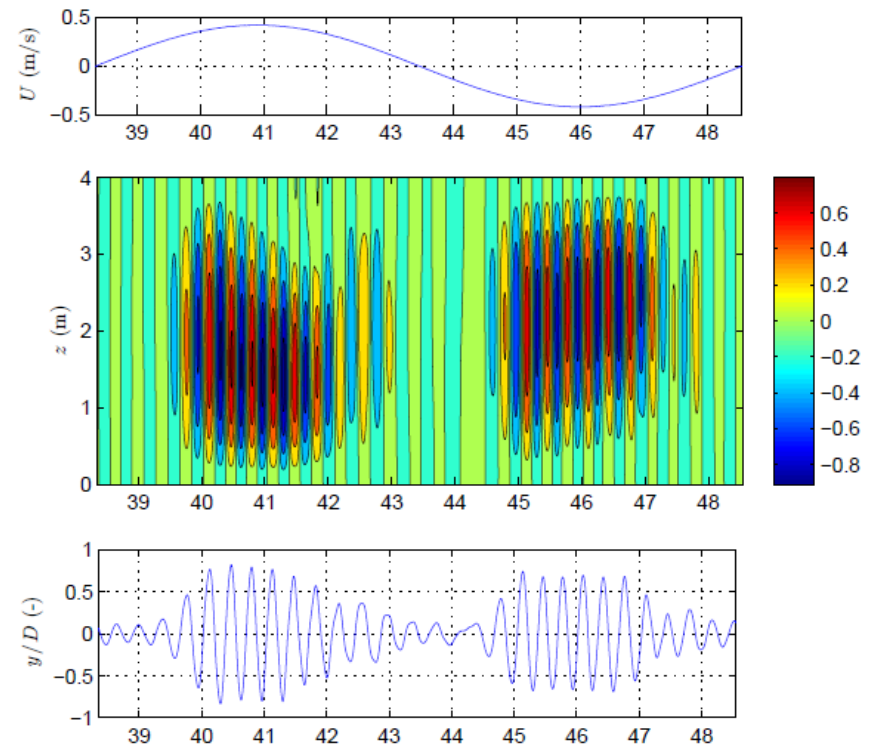
$$U_{r,\max} = \frac{U_{\max}}{f_1 D} = \frac{2\pi A_m}{T f_1 D} = \frac{KC}{T f_1}$$

Results

- Flexible cylinder in oscillating flow
- $KC = 178$, $U_{R,max} = 6.5$:



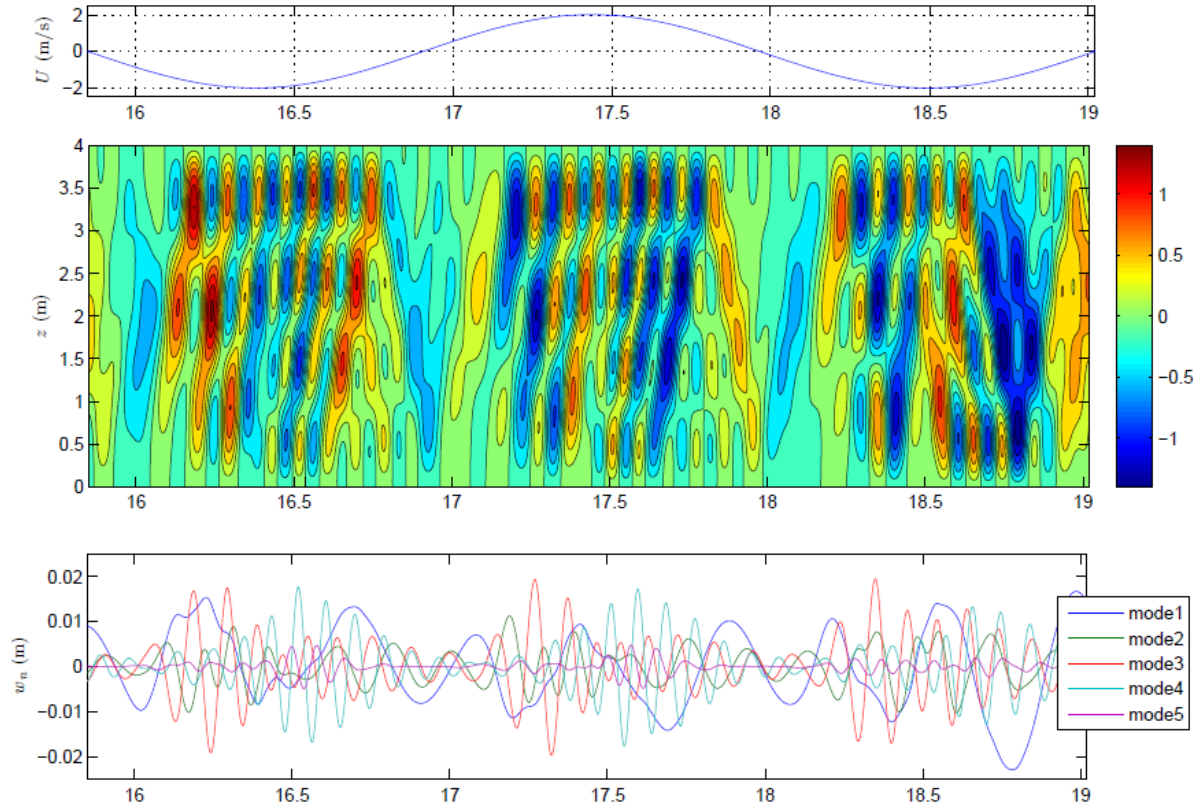
(a) Simulation



(b) Experiment

Results

- Flexible cylinder in oscillating flow
- Effect of increasing the reduced velocity:



Concluding remarks

- So far:
 - A time domain model of the hydrodynamic forces relevant to VIV has been established.
 - The model provides realistic results
- Future work:
 - How to combine the model with Morison's eq. to include drag forces? How does drag amplification occur?
 - Other PhD projects:
 - Tor Huse Knudsen: Interaction between VIV and internal flow (deep ocean mining)
 - Jan Vidar Ulveseter: Effect of nonlinear damping (soil or structural)

THANK YOU FOR YOUR ATTENTION!